

PFR

1974 - 1994

Operational Feedback

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PFR

1974 - 1994

Operational Feedback

Why bother?



PFR Operational Feedback

Operational **data** from past reactors
are necessary to **validate**
the **safety** of future reactors.

Examples –

Power coefficient of reactivity

Natural convection cooling

The Prototype Fast Reactor

1961-1966

Design

Preliminary Specification 1964

Sanction to construct 1966

Identification of NIV swelling 1966

1967-1974

Construction

Reactor roof weld cracks 1969-1971

1974-1994

Operation

Critical 1974

Full Power 1977

Evaporator leaks 1974-1981

Primary oil leak 1992

Closure 1994

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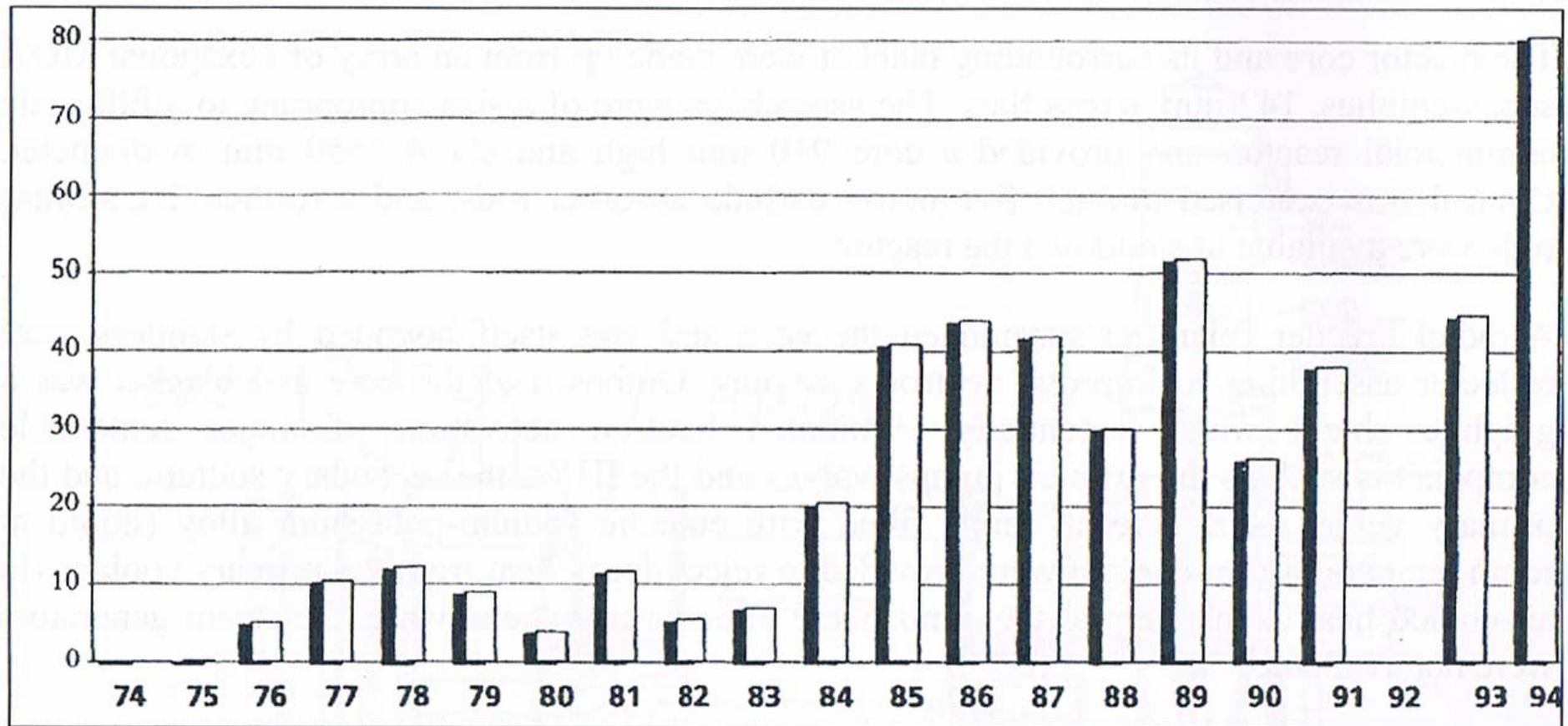
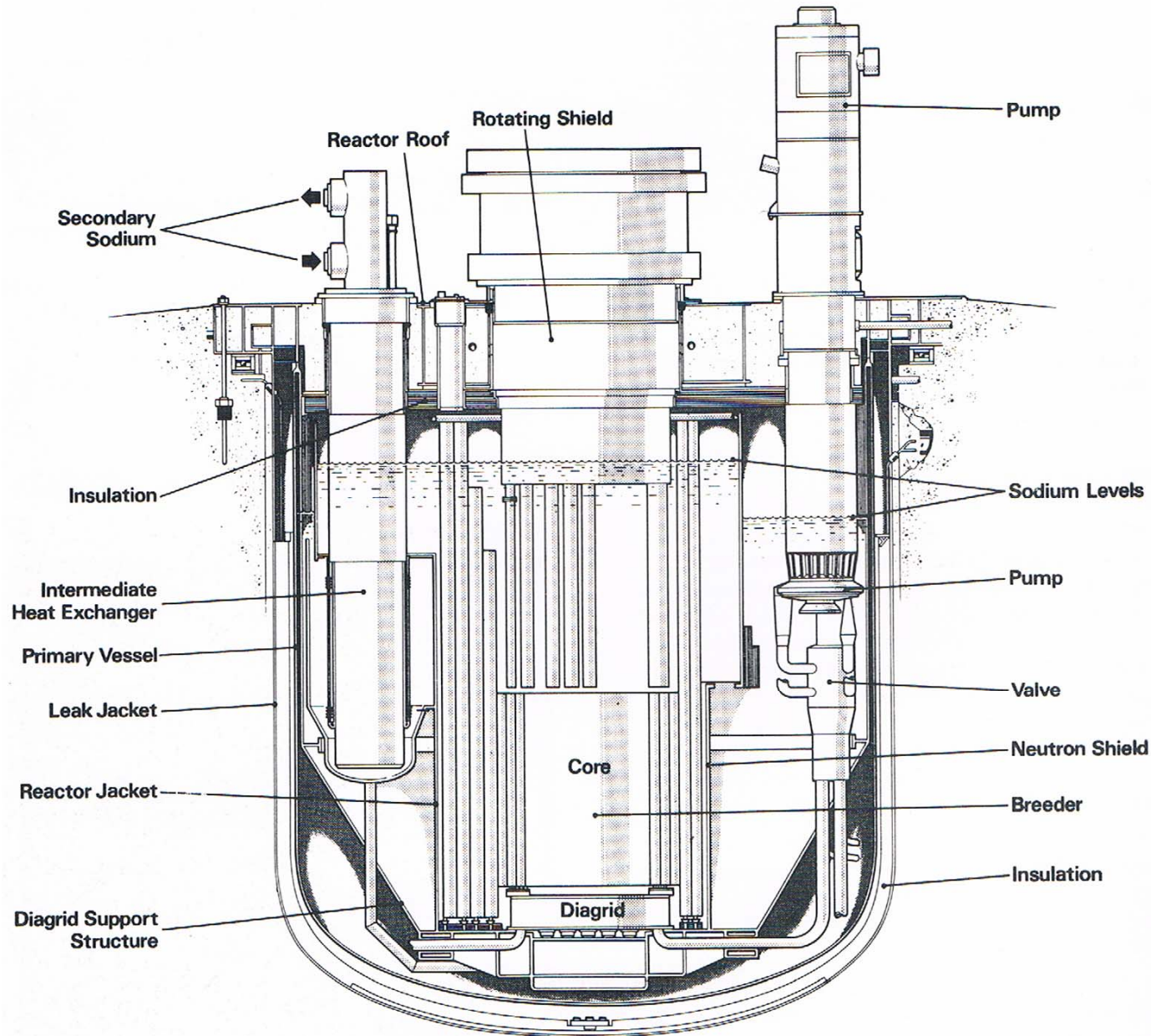


FIG. 2. PFR annual load factors 1974-1994
(1994 for three months' operation only-before decommissioning), %.

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**250 MW(e)
600MW(th)**

MOx fuel



PFR Operational Experiments

Coolant Inlet temperature coefficient of reactivity

Coolant Flow coefficient of reactivity

Power coefficient of reactivity

Natural convection cooling at low power
(Primary coolant pumps stopped)

Power Coefficient of Reactivity

Dependence of reactivity on power and coolant flow

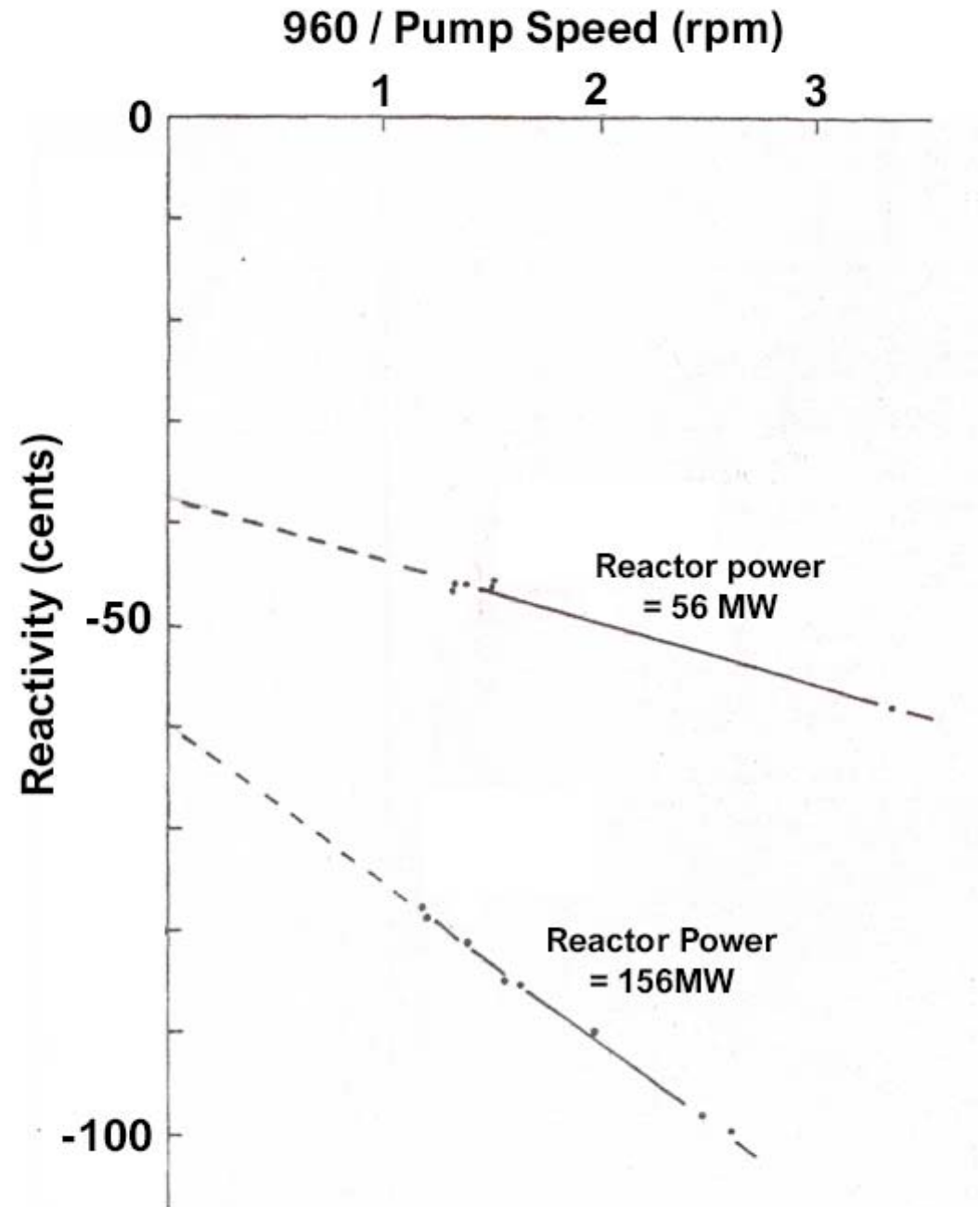
$$\partial\rho/\partial P = a(P) + bP/F$$

a depends on temperature of fuel
(Doppler and axial expansion)

b depends on expansion of core structure

PFR Power Coefficient of Reactivity

Measurements
of the
flow-dependent
term bP/F



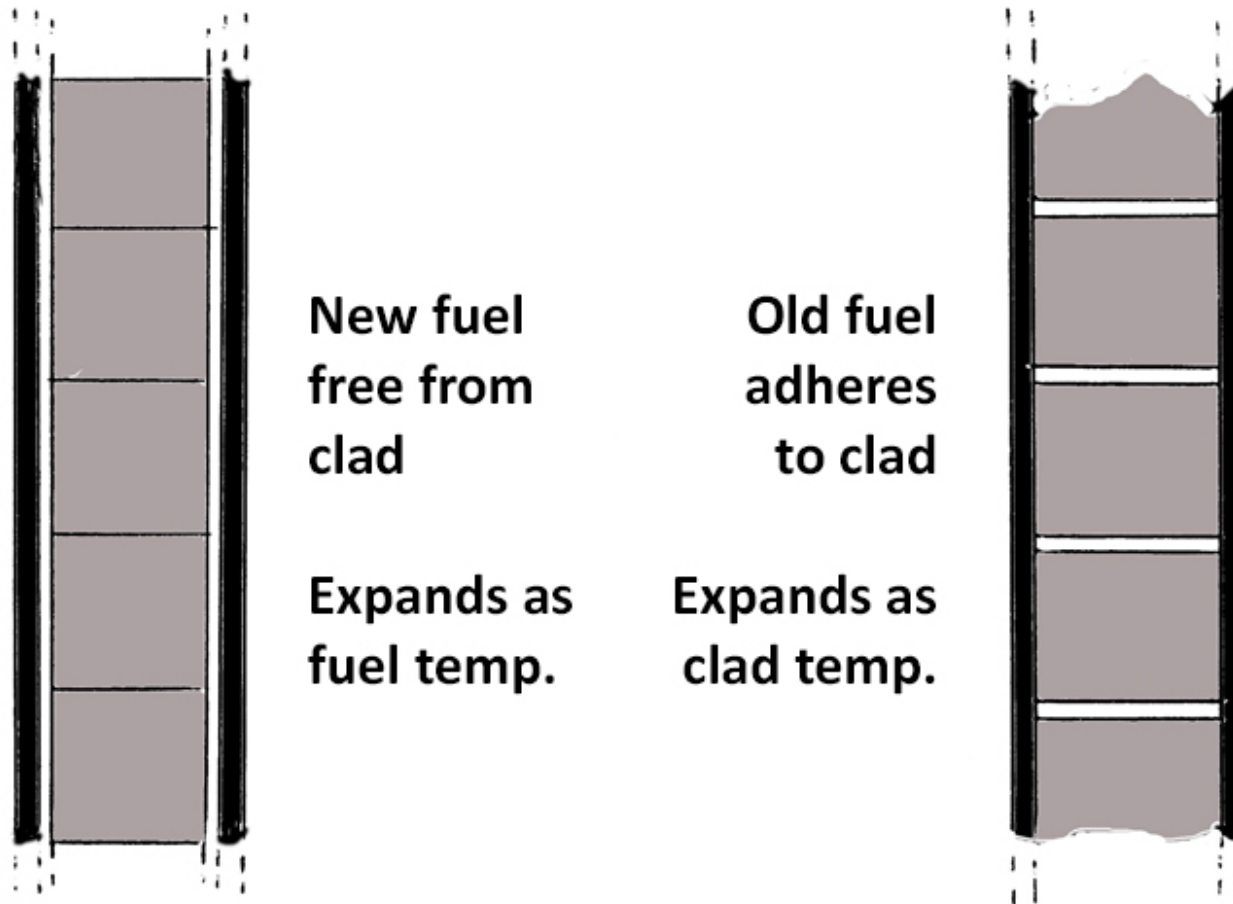
Power Coefficient of Reactivity

$$\rho_{\text{Doppler}} \approx - \ln(T_{\text{abs}})$$

The Doppler reactivity change varies roughly as
 $1/(\text{absolute temperature})$

Power Coefficient of Reactivity

Fuel axial expansion decreases with age



PFR Power Coefficient of Reactivity

Selected measurements of the
flow-independent term $a(P)$

Date	Power range MW(th)	Flow %	Power Coeff cents/MW	$a(P)$ cents/MW
Oct-75	16-50	30	-1.01 +/- 0.14	-0.48 +/- 0.14
	100-200	150	-0.76 +/- 0.04	-0.44 +/- 0.04
Aug-76	25-250	77	-0.58 +/- 0.02	-0.37 +/- 0.02
	10-455	90	-0.51 +/- 0.02	-0.33 +/- 0.02
Dec-78	195-170	88	-0.47 +/- 0.02	-0.36 +/- 0.02
	195-175	47	-0.54 +/- 0.02	-0.30 +/- 0.02
	240-280	90	-0.38 +/- 0.02	-0.26 +/- 0.02
	355-386	90	-0.44 +/- 0.02	-0.20 +/- 0.02
Mar-85	590-620	100	-0.20 +/- 0.05	-0.07 +/- 0.05
	470-620	100	-0.23 +/- 0.03	-0.10 +/- 0.03
	310-470	100	-0.24 +/- 0.03	-0.11 +/- 0.03

PFR Power Coefficient of Reactivity

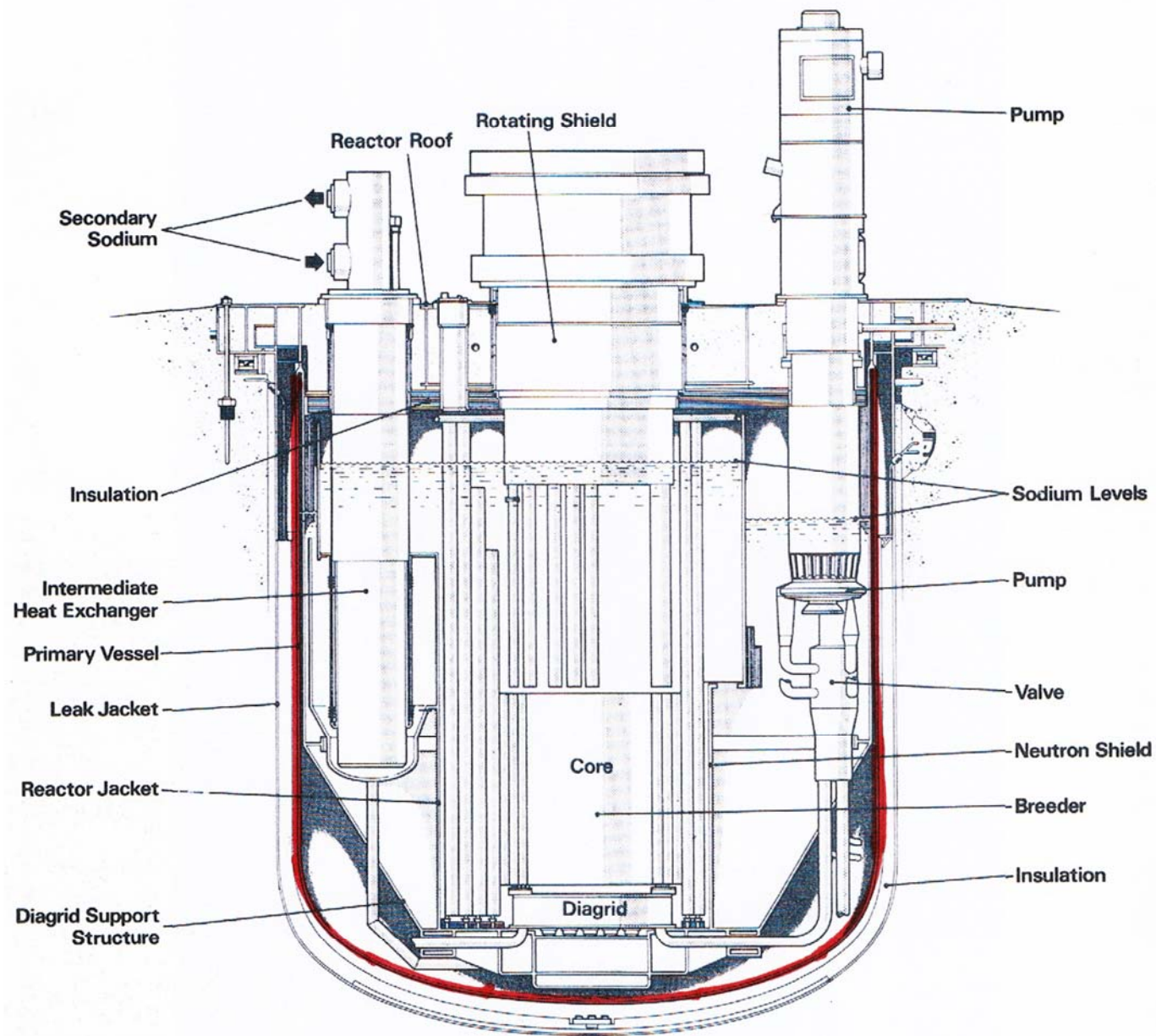
$$\partial\rho/\partial P = a(P) + b/F$$

Experimental data

a decreases with increasing power
(due to Doppler)

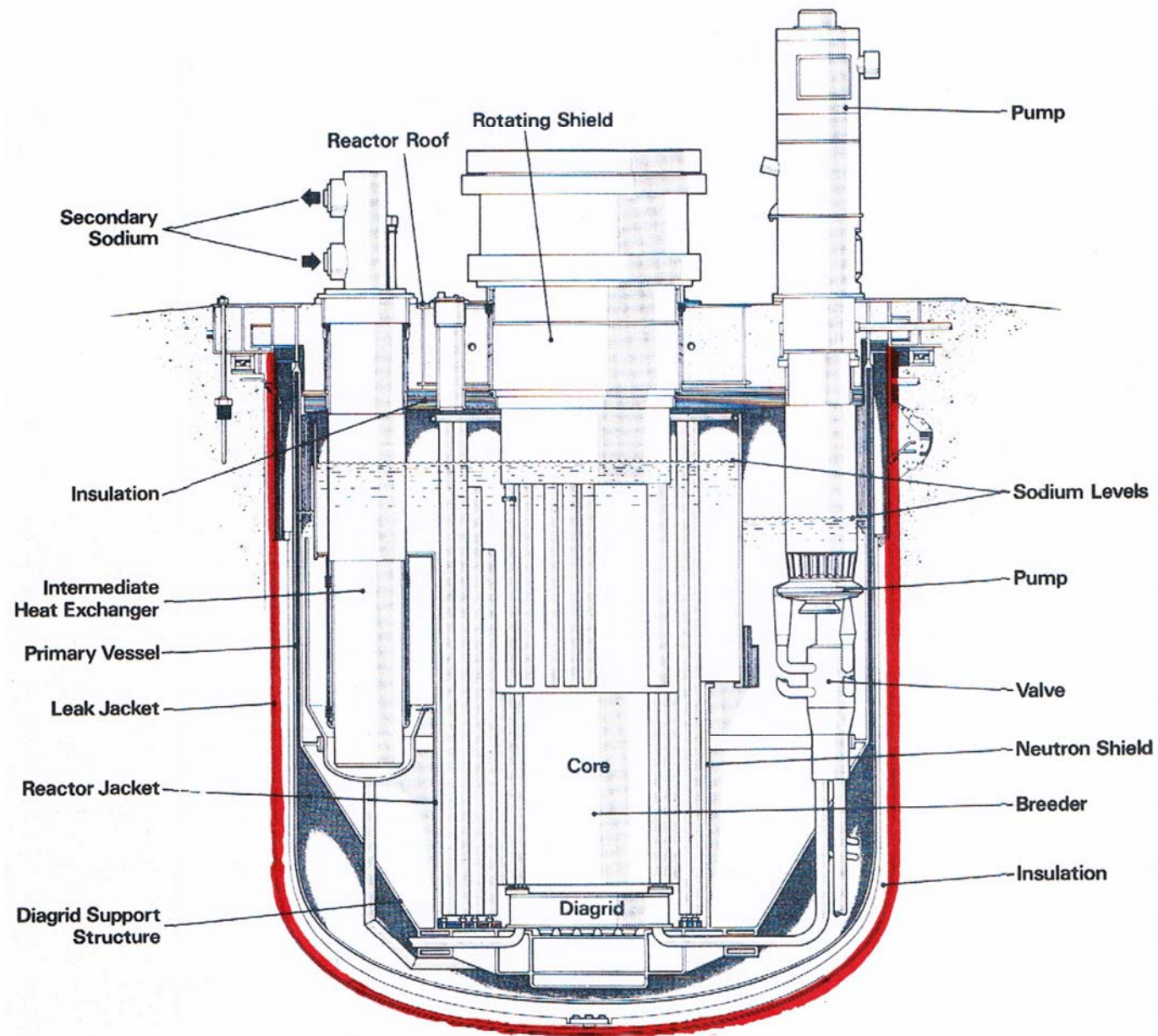
a decreases with burnup of fuel
(due to adhesion of fuel to clad)

PFR Vessel



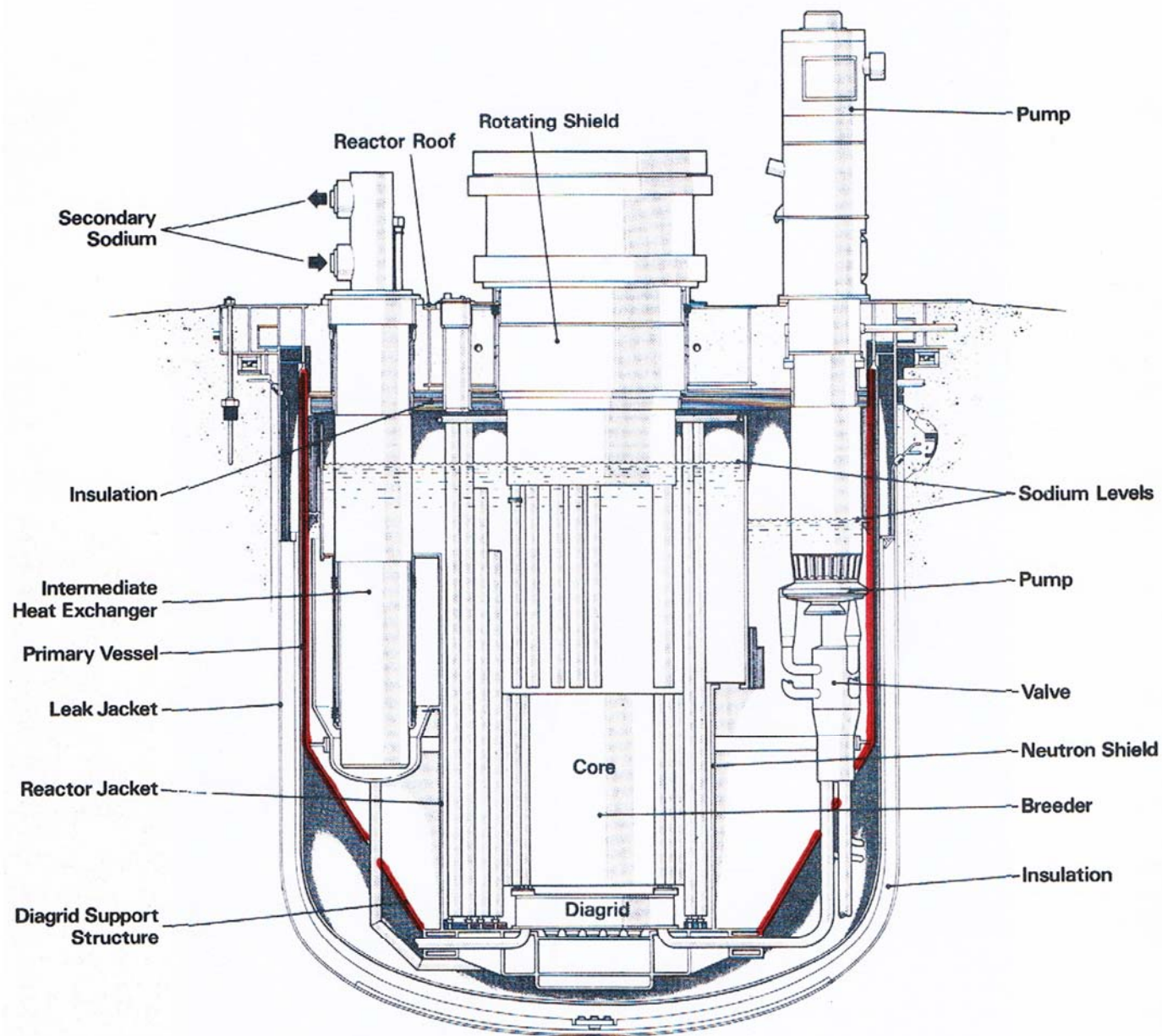
Reactor Vessel

PFR Vessel



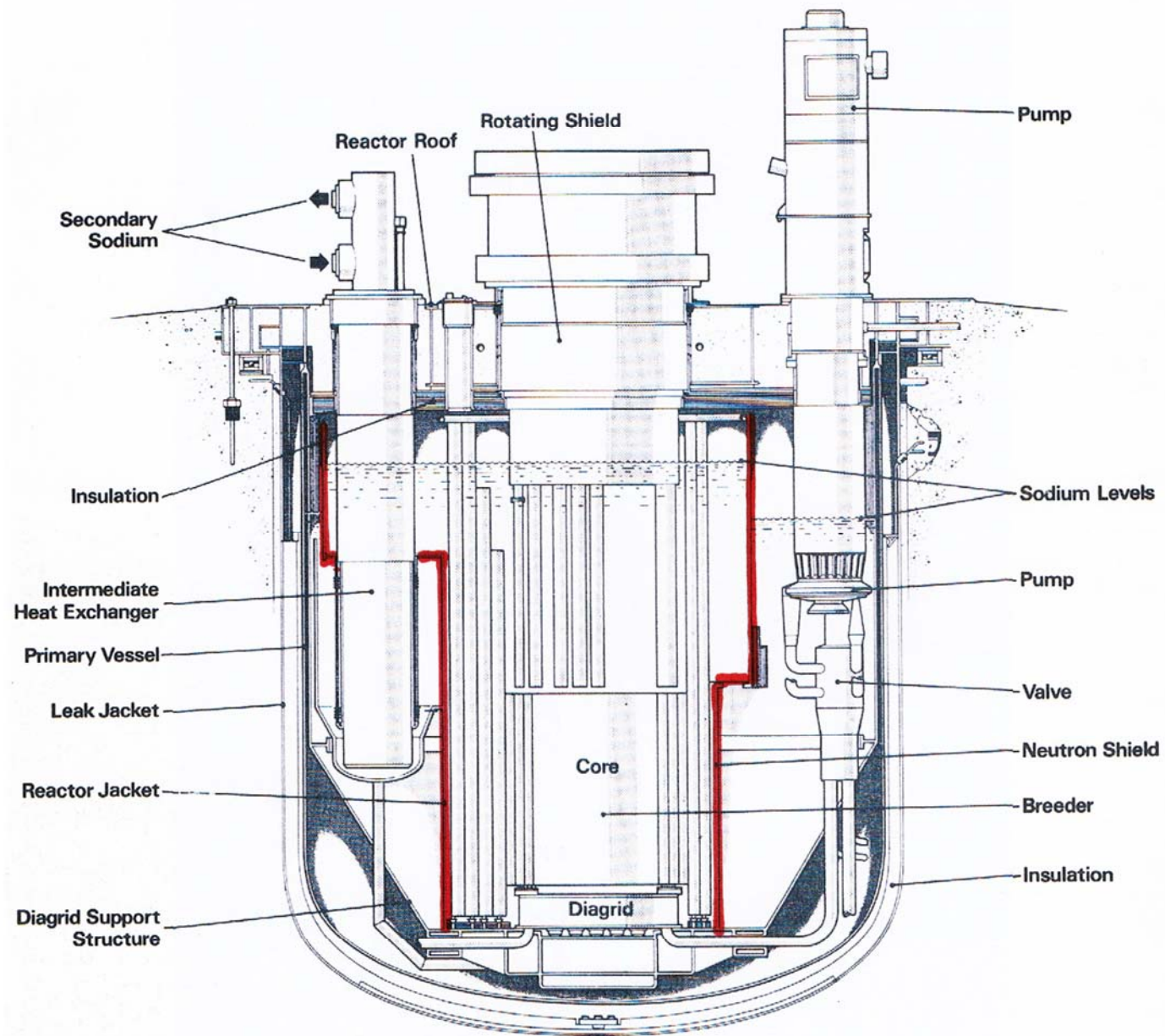
Leak Jacket

PFR Vessel



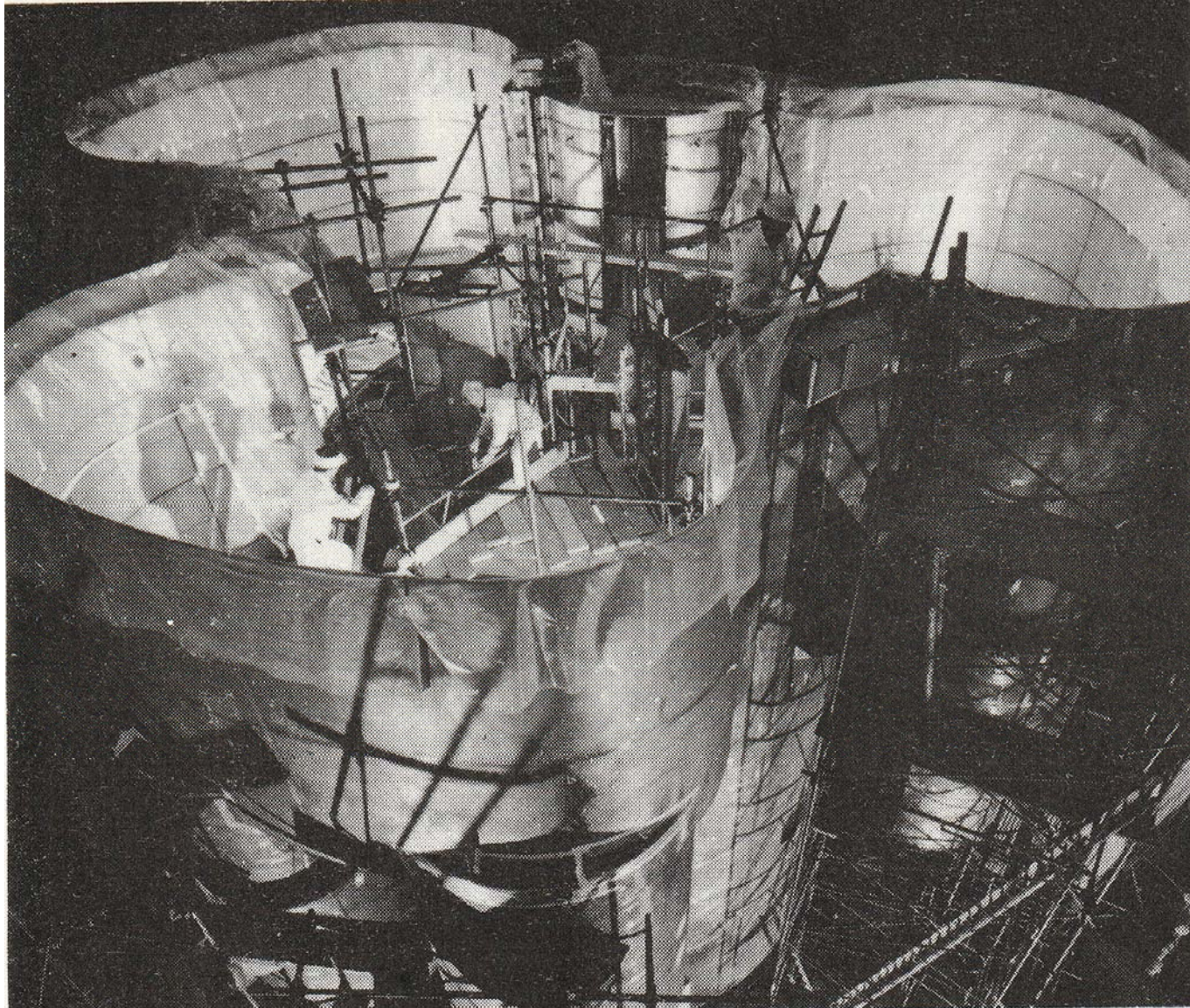
Diagrid Support

PFR Vessel



Reactor Jacket

PFR Reactor Jacket during construction



PFR Natural Convection Tests

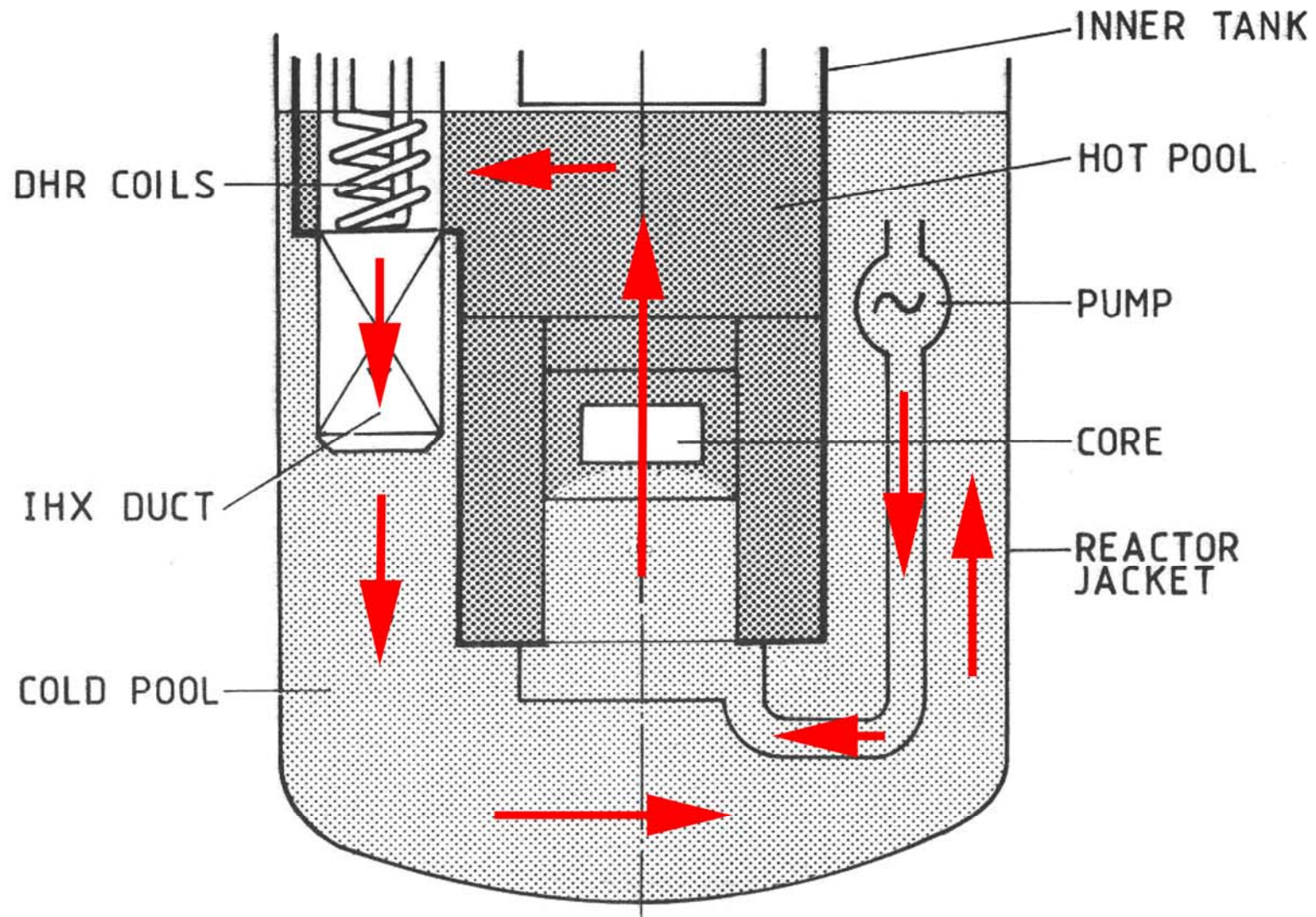
Coolant pumps de-energised (free to rotate)

Reactor critical at low power (~ 10 MW)

Decay Heat Rejection loops inactive, then active

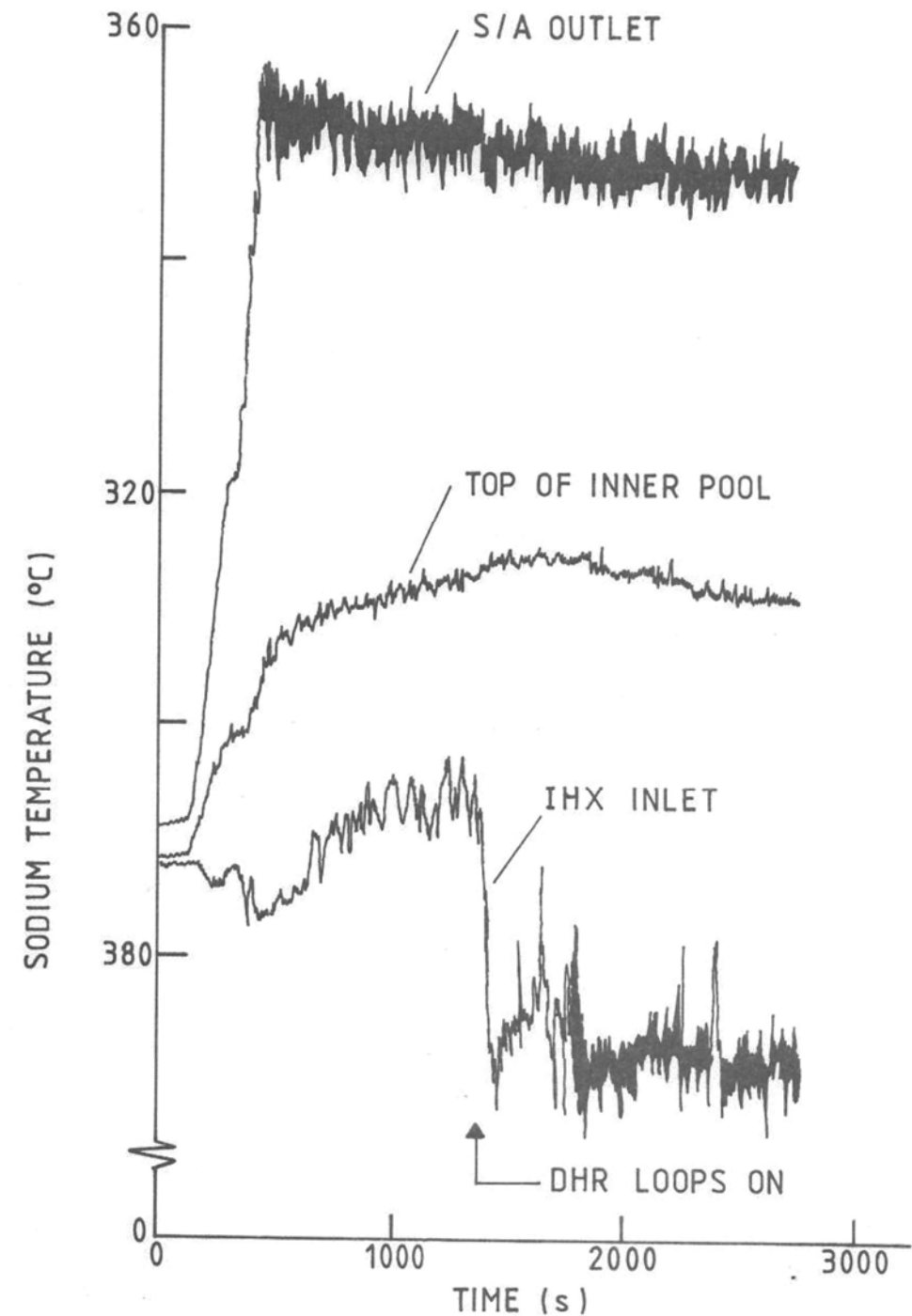
PFR Natural Convection Tests

Expected Flow Pattern



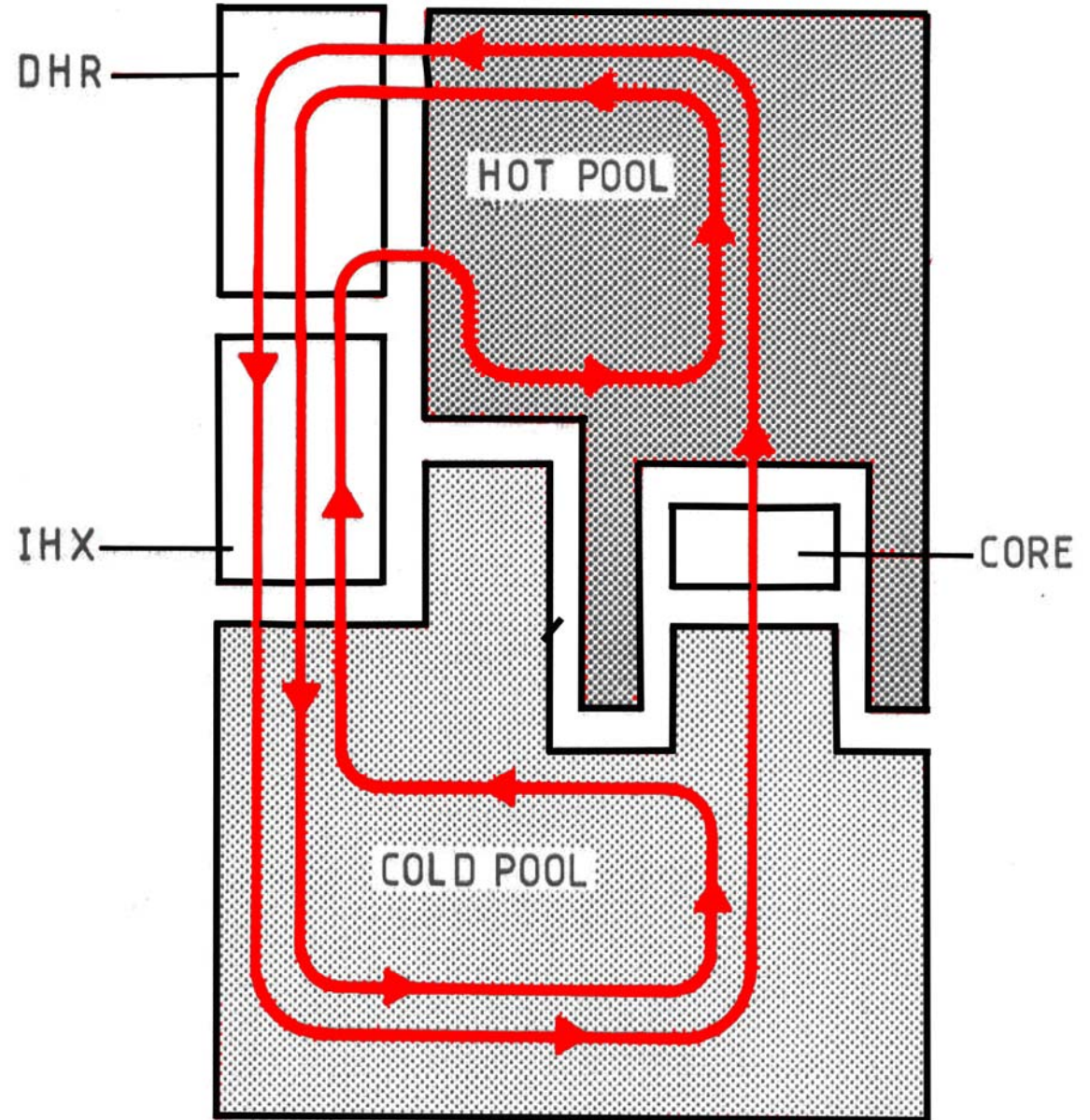
PFR Natural Convection Tests

Observed Temperatures



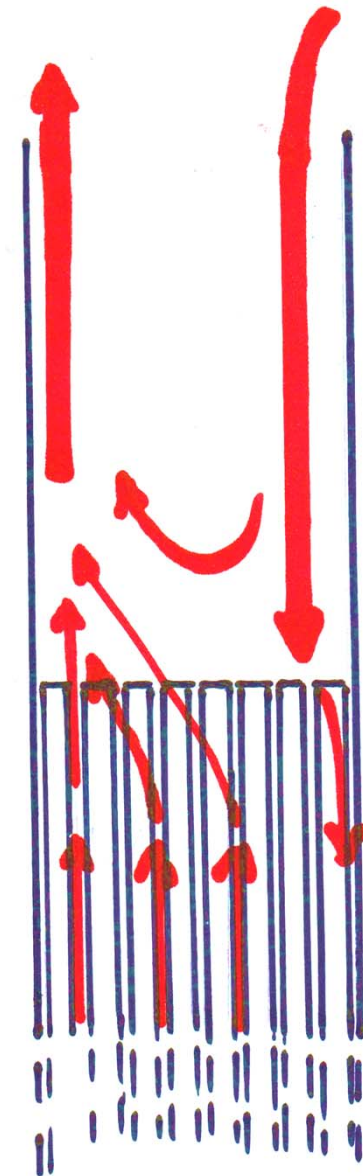
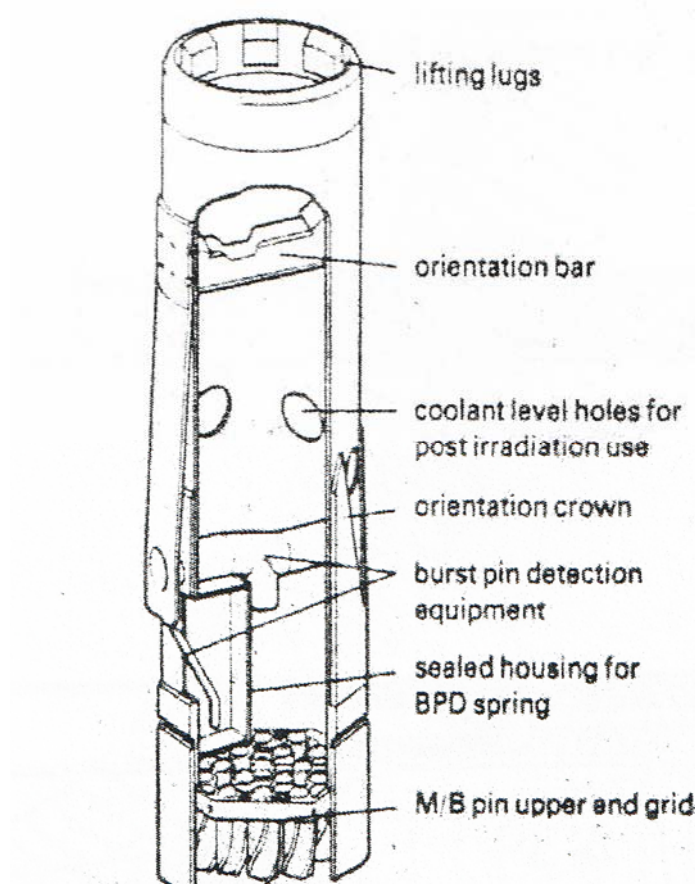
PFR Natural Convection Tests

Deduced Main Flow
Pattern



PFR Natural Convection Tests

Subassembly Outlet Conjectured Flow Pattern



Conclusion

Operational Feedback is valuable.

Safety parameters such as reactivity coefficients and natural convection flow patterns are affected by complex conditions in an operating reactor.

Therefore design predictions need validation by data from plant operation.