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MOX fuel safety and performances

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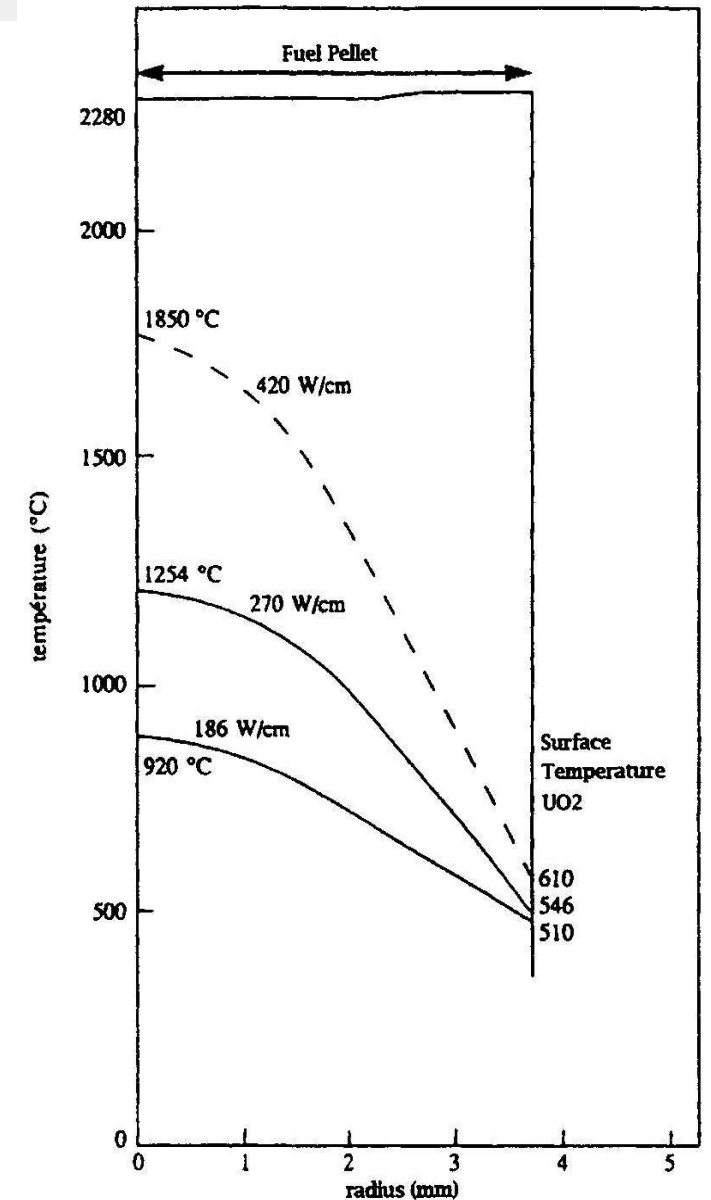
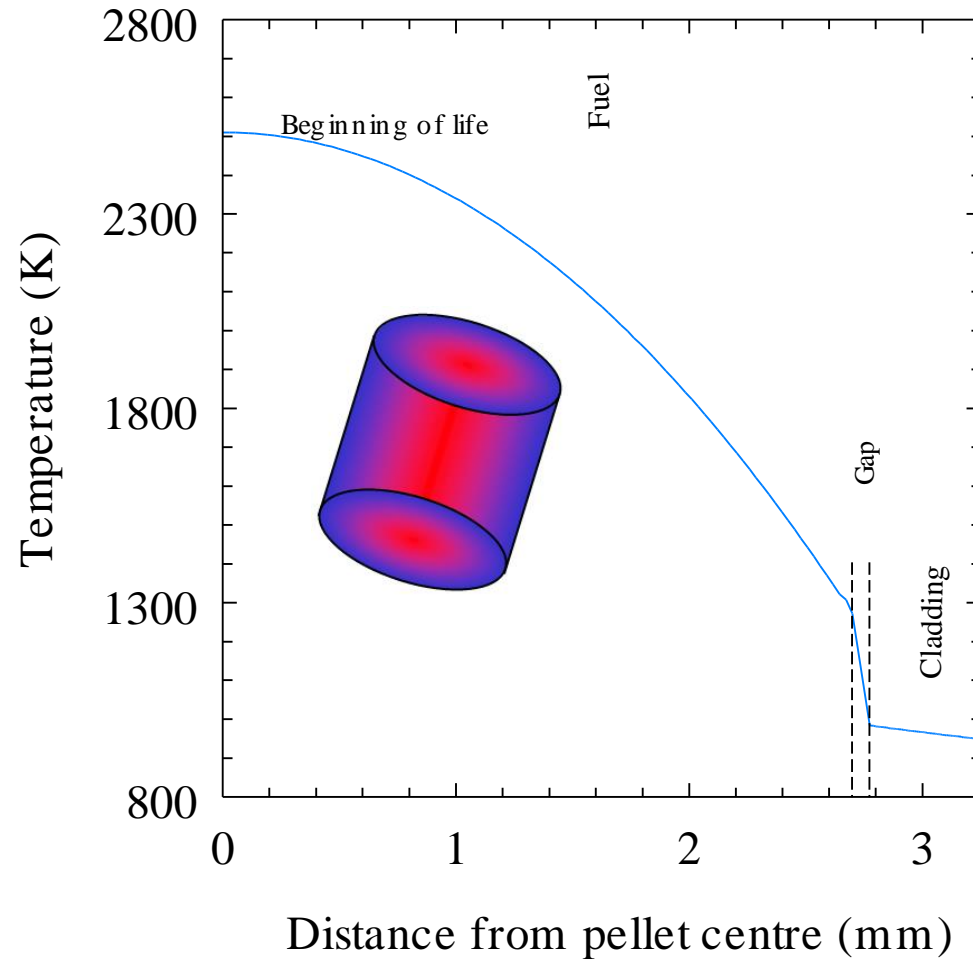


Motivations for using MOX fuel

- Oxide fuels have higher melting points and lower thermal expansion than metallic fuels, carbides and nitrides, but have a lower thermal conductivity
- **MOX fuel demonstrated a good behaviour** up to **very high burn-ups** (15 at.%), during the ***fuel cycle***, drawbacks are *a high fission gas release*, ***low density of fissile atoms*** and the ***compatibility with sodium***.
- *Metallic fuels, carbide or nitrides* have a higher conductivity (lower irradiation temperature), but higher **swelling** and still large FGR.



Temperature gradient in a fuel pellet, FBR vs. LWR





- The target burn-up for FBR MOX fuels is about 15 at. %, which is considerably higher than for LWR fuels and will result in the formation of a large amount of fission products:
- forming a solid solution with the matrix (Y, La, Ce, Pr, Nd, Pm, Sm, Eu)
- oxide precipitates (Ba, Zr, Sr, Cs), appear as “grey phases”
- metallic precipitates (Mo, Ru, Tc, Rh, Pd),
- volatile (Cs, Te, I) which migrate to the pellet periphery
- gaseous (Xe, Kr).

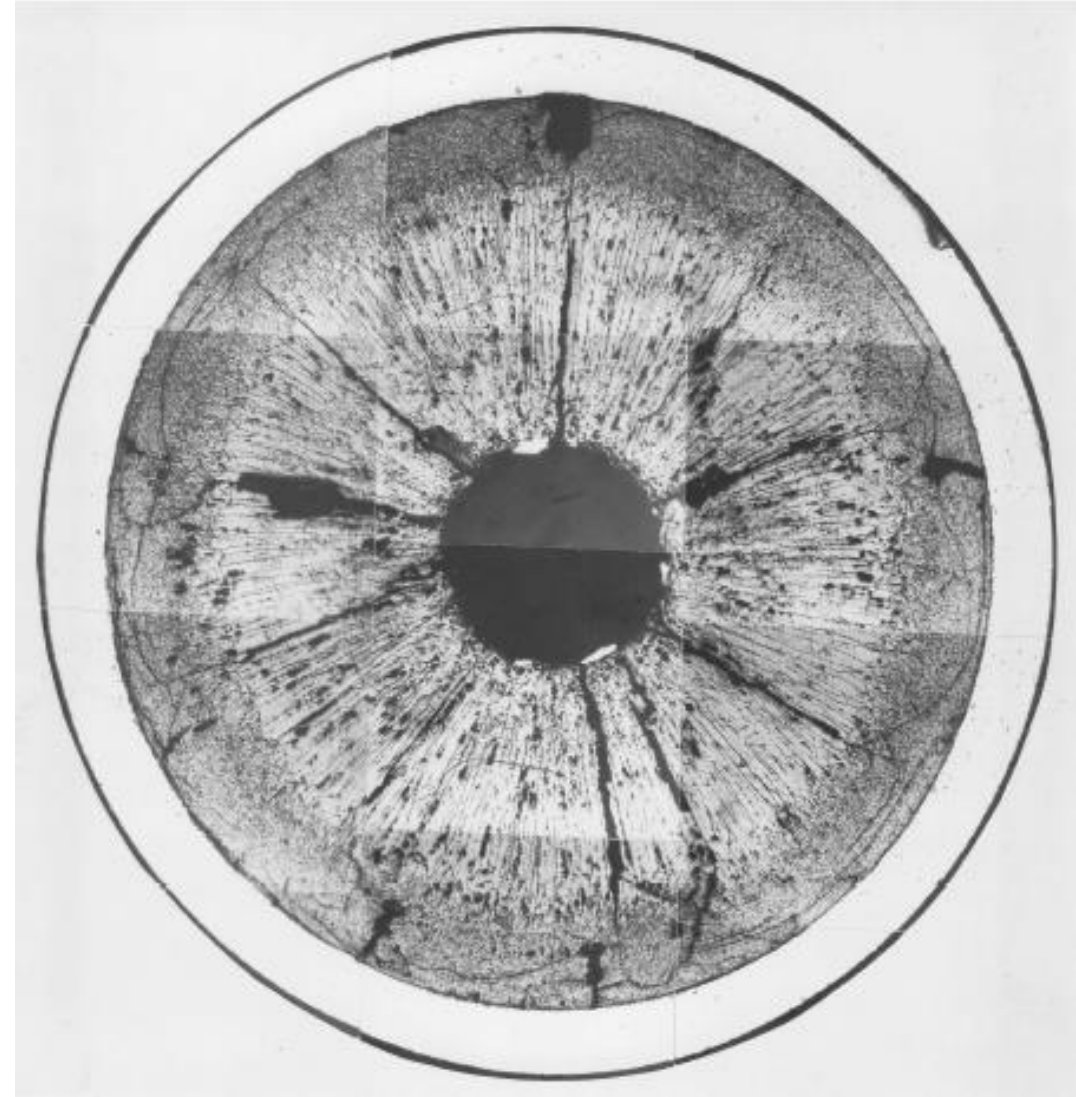
Irradiation behavior different from LWR due to the high temperatures.

- Fuel restructuring
- Redistribution of Pu, Oxygen
- Fission gas release
- The JOG
- Impact of redistribution on properties



Restructuring

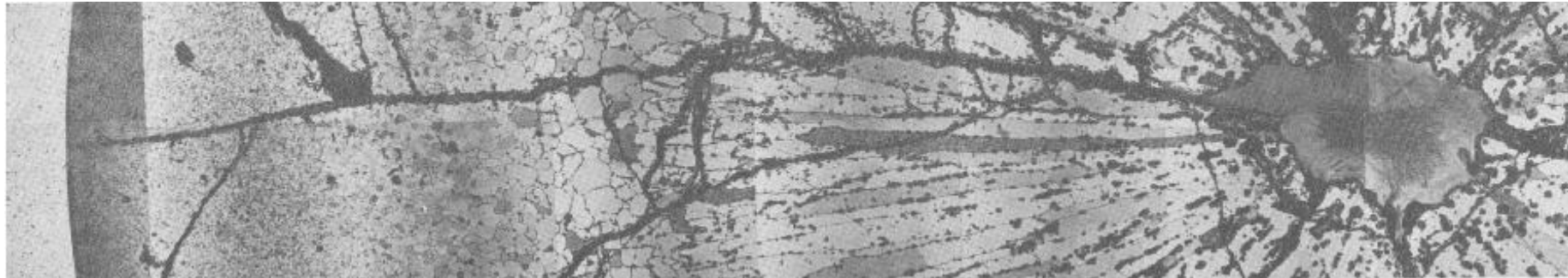
The initial microstructure (grains size, porosity) is strongly modified during irradiation as a result of restructuring.





Restructuring

- **FBR, T** >2000° C : extensive restructuring



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4 regions:

Grains: as fabricated/RIM → equiaxed → columnar → central hole
T < 1200° C
dense
transport of the as fabricated porosity

Pellet cracking, Grain growth, Columnar grains and central hole (initial or forms within minutes)

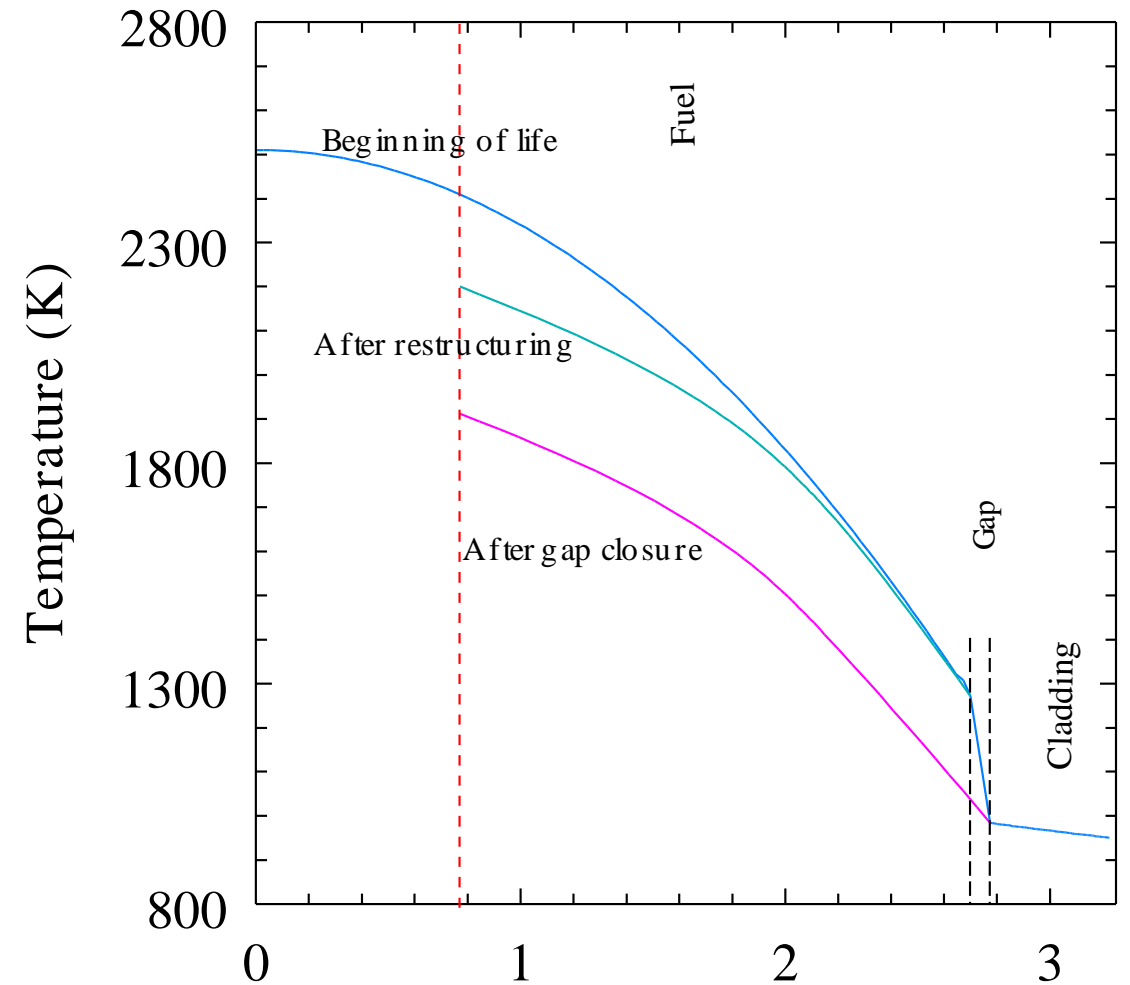
- **LWR, T** < 1200° C :

RIM **structure (HBS, grains subdivision)** at high burn-up at pellet periphery and in the Pu rich-agglomerates of heterogeneous MOX



Restructuring

- Central hole limits the maximum temperature reached and avoids melting at beginning of life
- Central temperature decreases after to gap closure





Restructuring

Lenticular pores form under steep temperature gradients in fast reactor (U,Pu)O₂ fuel

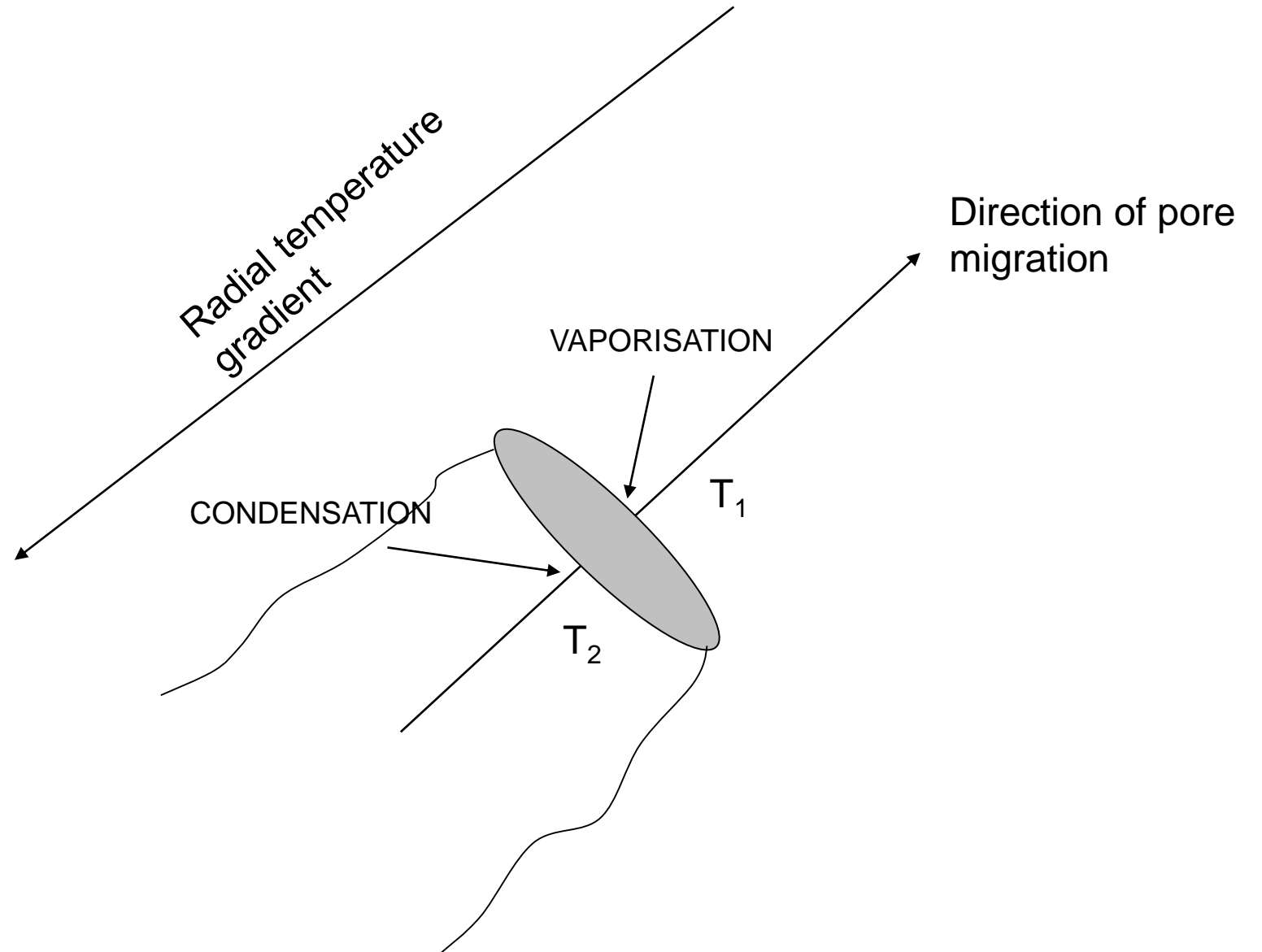
Pores and cracks move towards central void via evaporation/condensation mechanism





Restructuring

Vaporisation
condensation (pore
diffusion)





Redistribution

Redistribution of :

- plutonium : enrichment in the central area
- oxygen : migrates towards the low temperature region of the pellet
- minor actinides (if MA recycling): Am migrates to the center
- fission products (→ JOG)

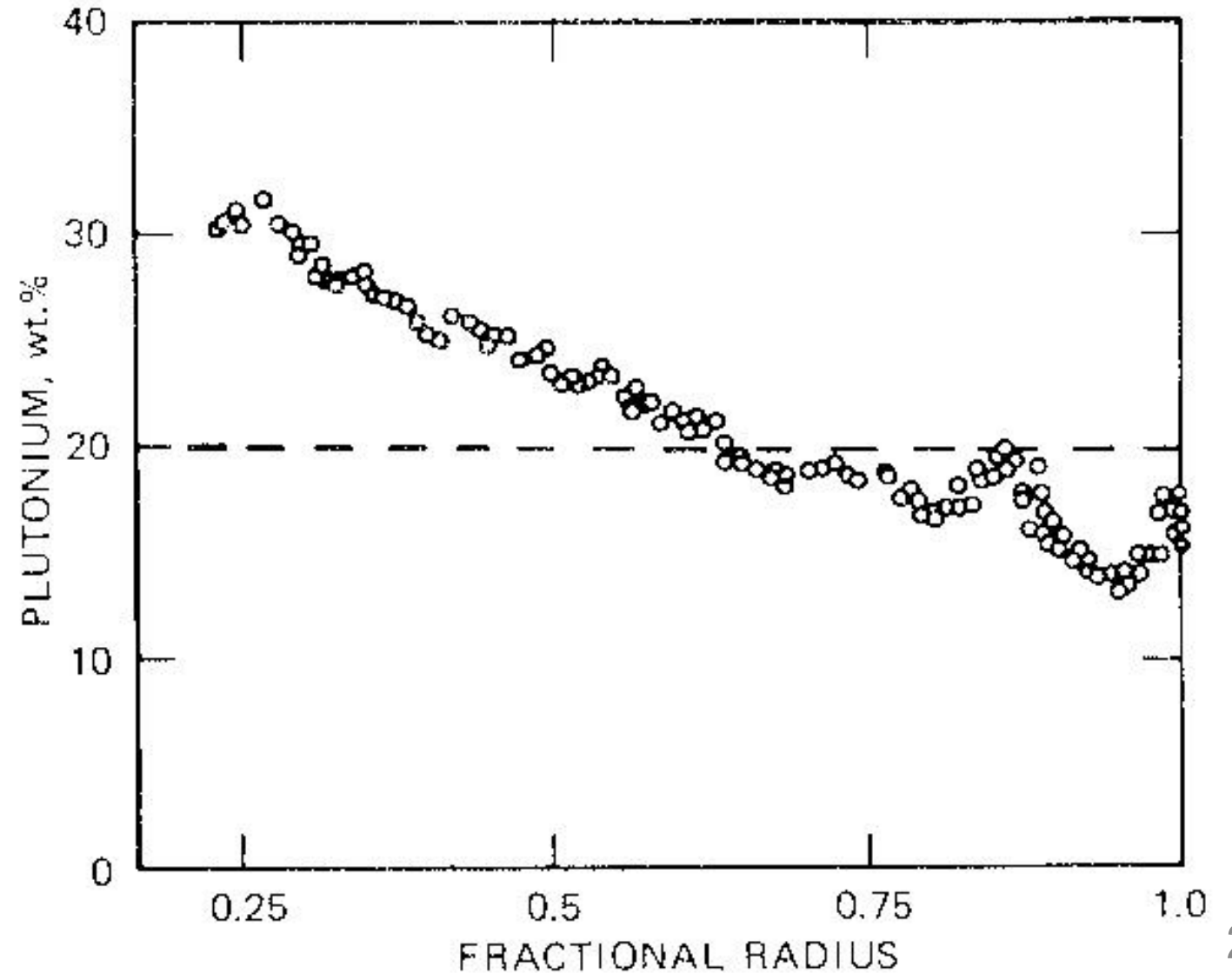
Possible mechanisms:

- Atomic diffusion (thermal and athermal): bulk diffusion
- Grain boundary and surface diffusion
- Vaporisation condensation (pore diffusion)



Redistribution of Pu

Pu redistribution in FBR fuel after a burnup of 5% at 660 W/cm:
enrichment in the center



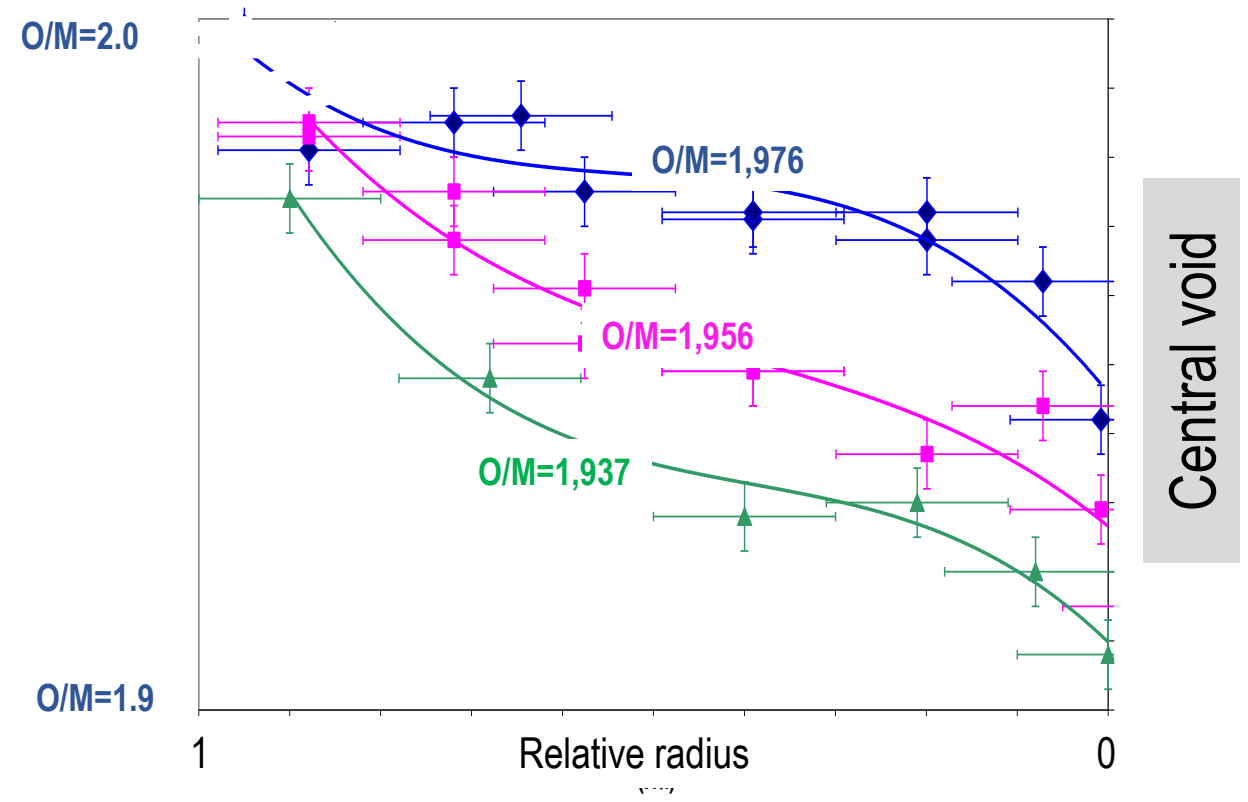
Ref.: Olander



Redistribution of Oxygen

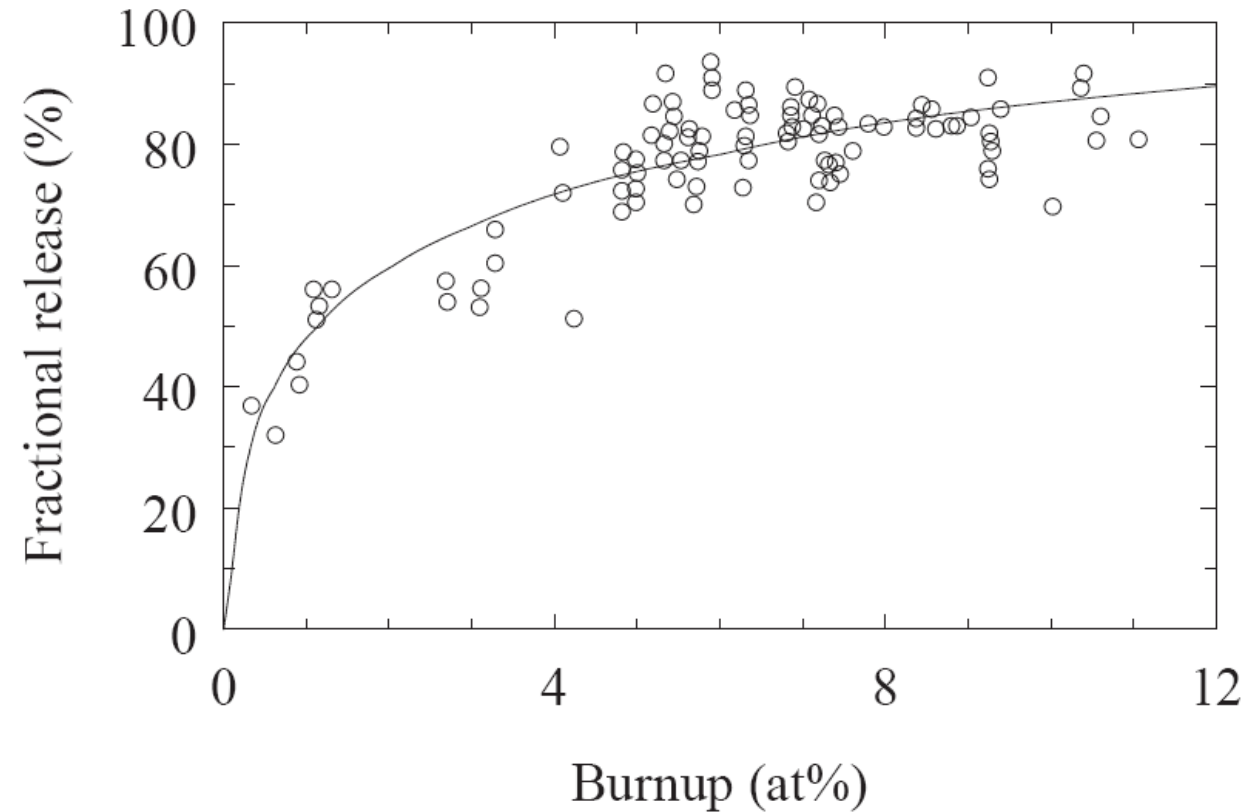
Fresh fuel is fabricated hypostoichiometric.

During irradiation, oxygen is rapidly redistributed radially



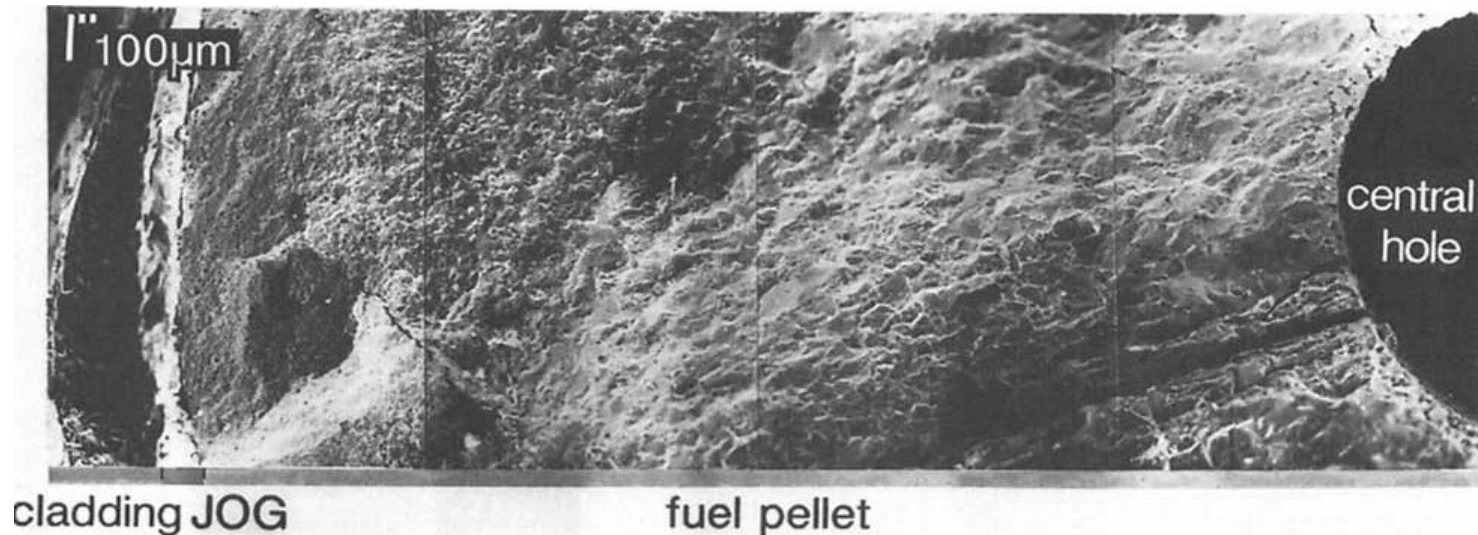
Fission Gas release

- High fission gas release (FGR) already at low burn-up: fuel pin must have sufficient free volume
- Large grains are favourable to fission gas retention, but the diffusion coefficients are very high (high T)
- Fission gas is mainly located at the pellet periphery, almost no gas remains close to center
- In typical PWR fuel, FGR is below 2% at the burn-up of 50 GWd/t

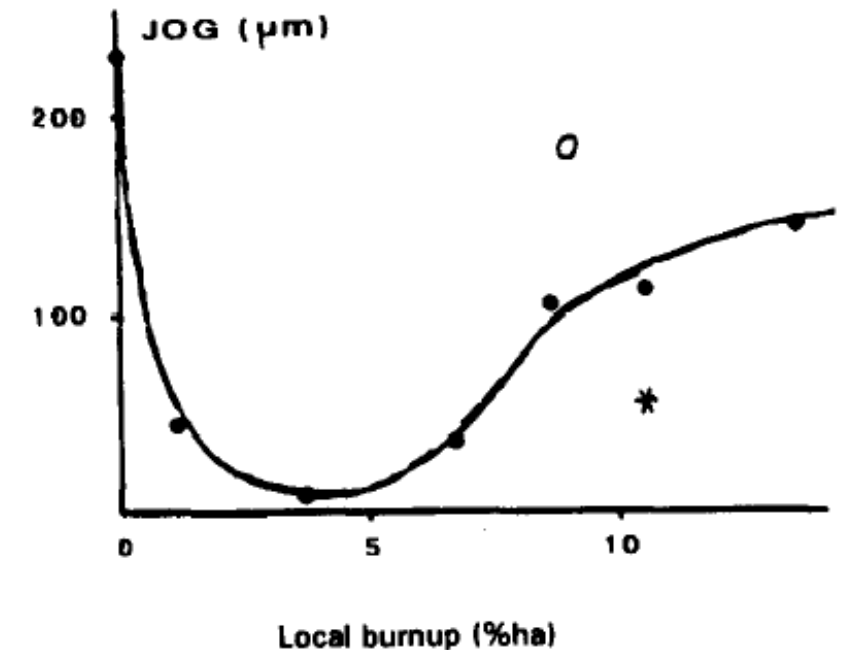


The Joint Oxide-Gaine, JOG:

- For burn-ups above about 5 to 7 at.%, some fission products are released and compounds accumulate as a solid medium in the gap.
- Forms in the hotter regions of the fuel pin, thickness increasing with burn-up up to 150 to 300 μm



- Evolution of the gap:
 - 1 - below about 5 at.%, gaseous and decreasing
 - 2 – about 5 to 10 at.%; increasing rapidly, it is filled with JOG
 - 3 – above 10 at.%; slower increase
- JOG contains neither U nor Pu. It is an oxide phase mainly with Mo and Cs, but Ba, Pa, Cd, I, Te are also present. Mo has left the noble metal precipitates.
- Pellet–cladding mechanical interaction (PCMI) does not take place during the first years of irradiation, and then remains moderated, even less with annular pellets



- No JOG in the lower part of the fissile column, where T is lower
- The exact composition of the JOG is not known, it varies axially and azimuthally in the pin, depending on local temperatures, oxygen potential...
 - > fuel properties like conductivity are expected to vary accordingly!
- The thermal conductivity of the JOG (Cs_2MoO_4 , ...) is 5 to 10 times lower compared to the fuel matrix
- JOG formation induces a decrease of the matrix swelling.



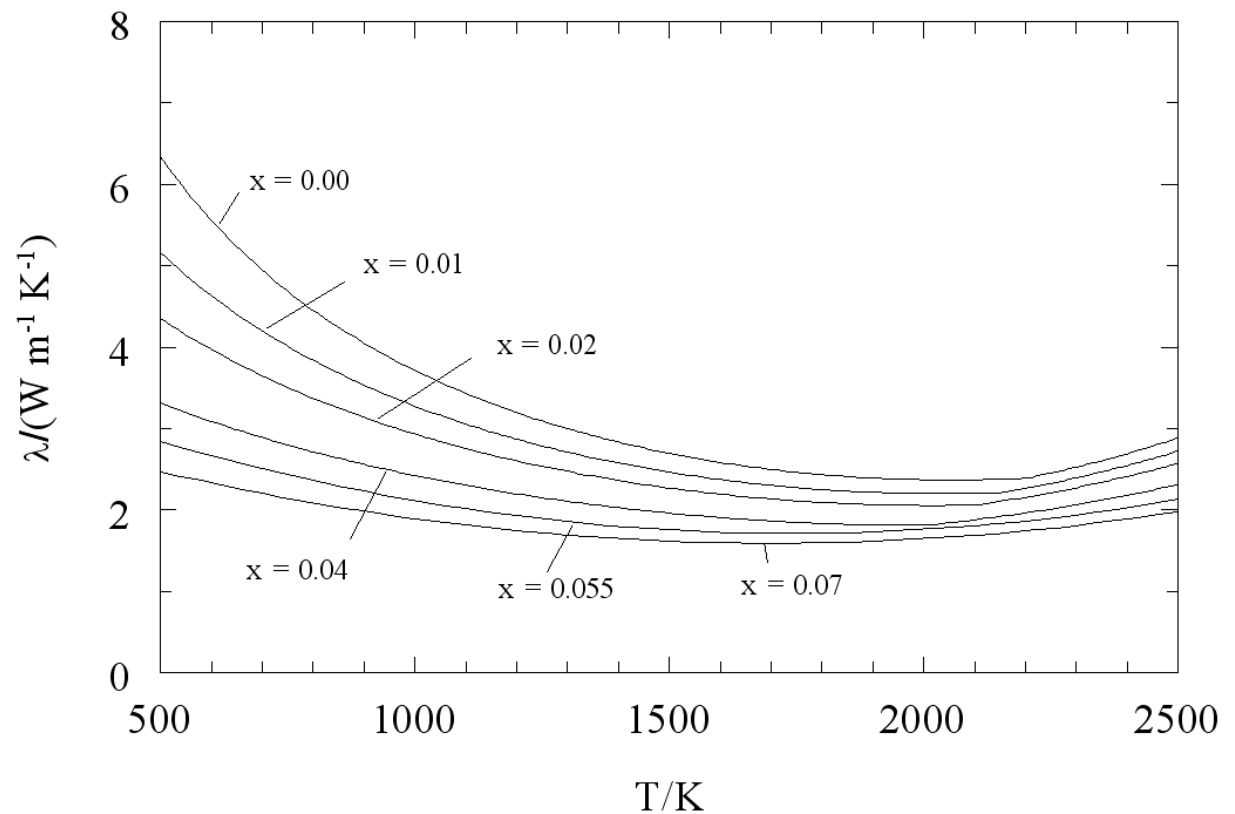
Impact of redistribution of properties

- Pu, O redistribution have an impact on the fuel properties: melting point, thermal conductivity which will depend on radial position.

Locally, conductivity depends on:

- Temperature
- Burn-up
- FP content
- O/M
- Pu content
- Microstructure

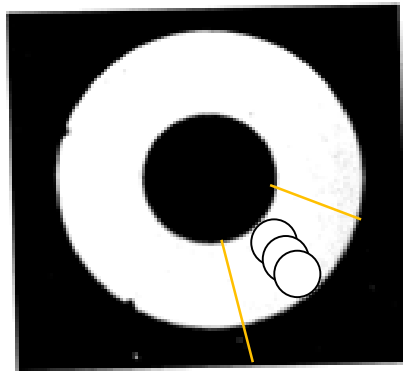
⇒ Modelling is required, more challenging than in LWR



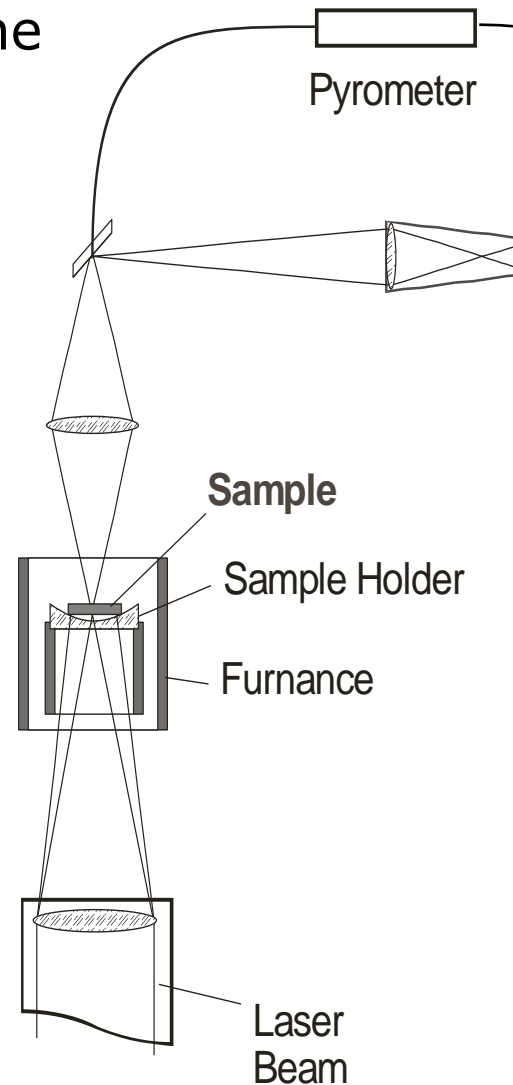


Thermal diffusivity

Local measurement of the thermal diffusivity

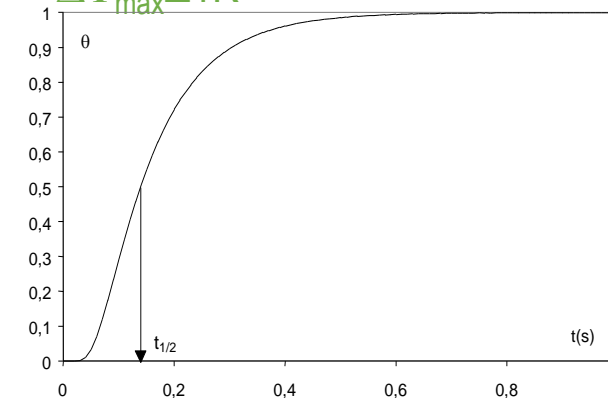


A heat pulse is produced by the laser on the front face



Rear face thermogram :

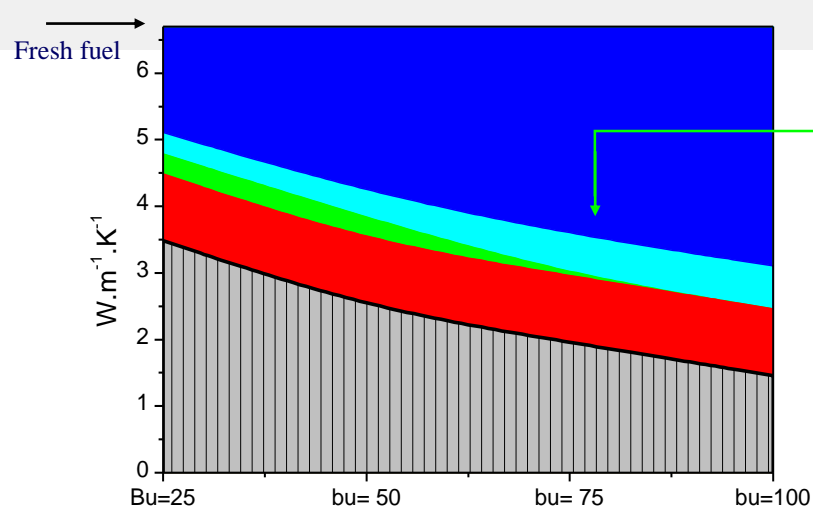
$\Delta T_{\max} \cong 1\text{K}$



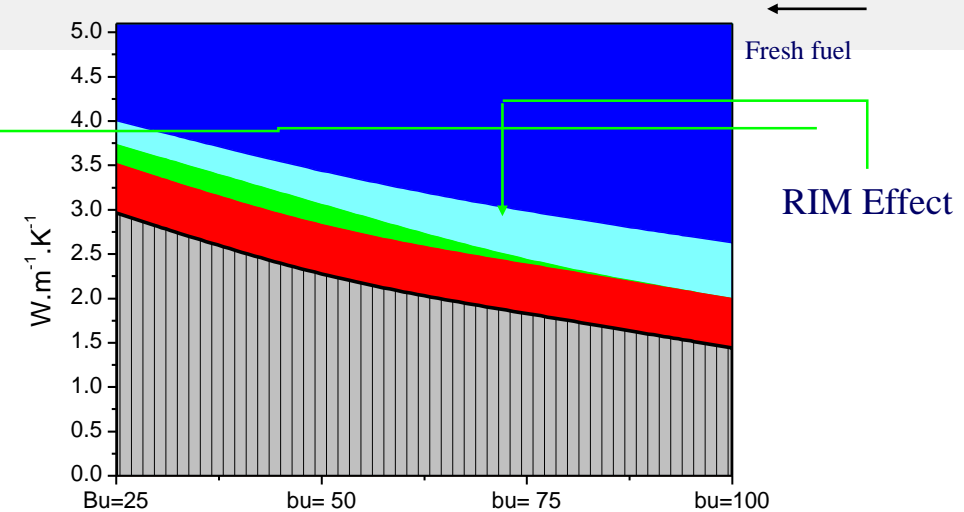
The temperature increase of the rear face is recorded



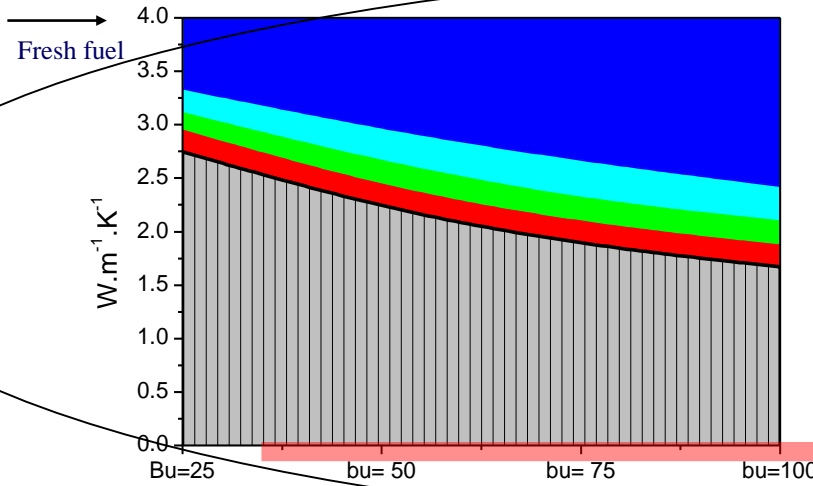
Contributions to the thermal conductivity decrease in irradiated (U,Pu)O₂



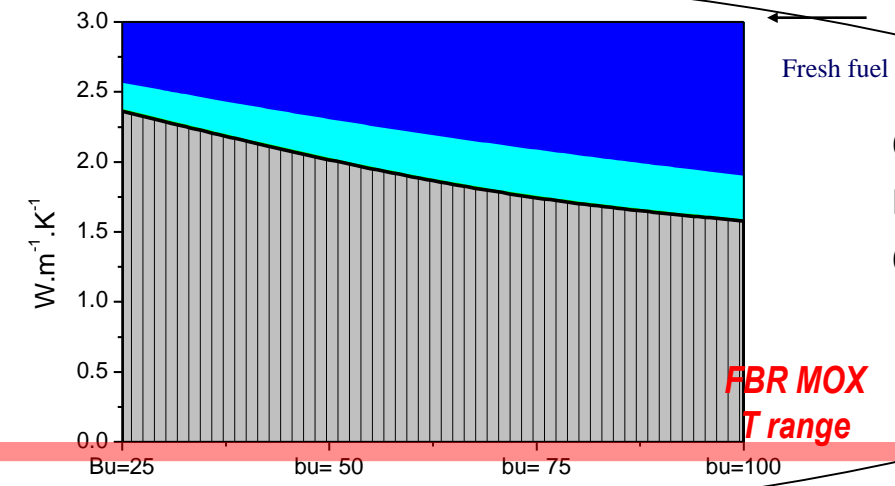
Tirr= 500K, evaluation at 500K



Tirr= 750K, evaluation at 750K



Tirr= 1000K, evaluation at 1000K



Tirr= 1450K, evaluation at 1450K

extensive FGR and recombination of point defects

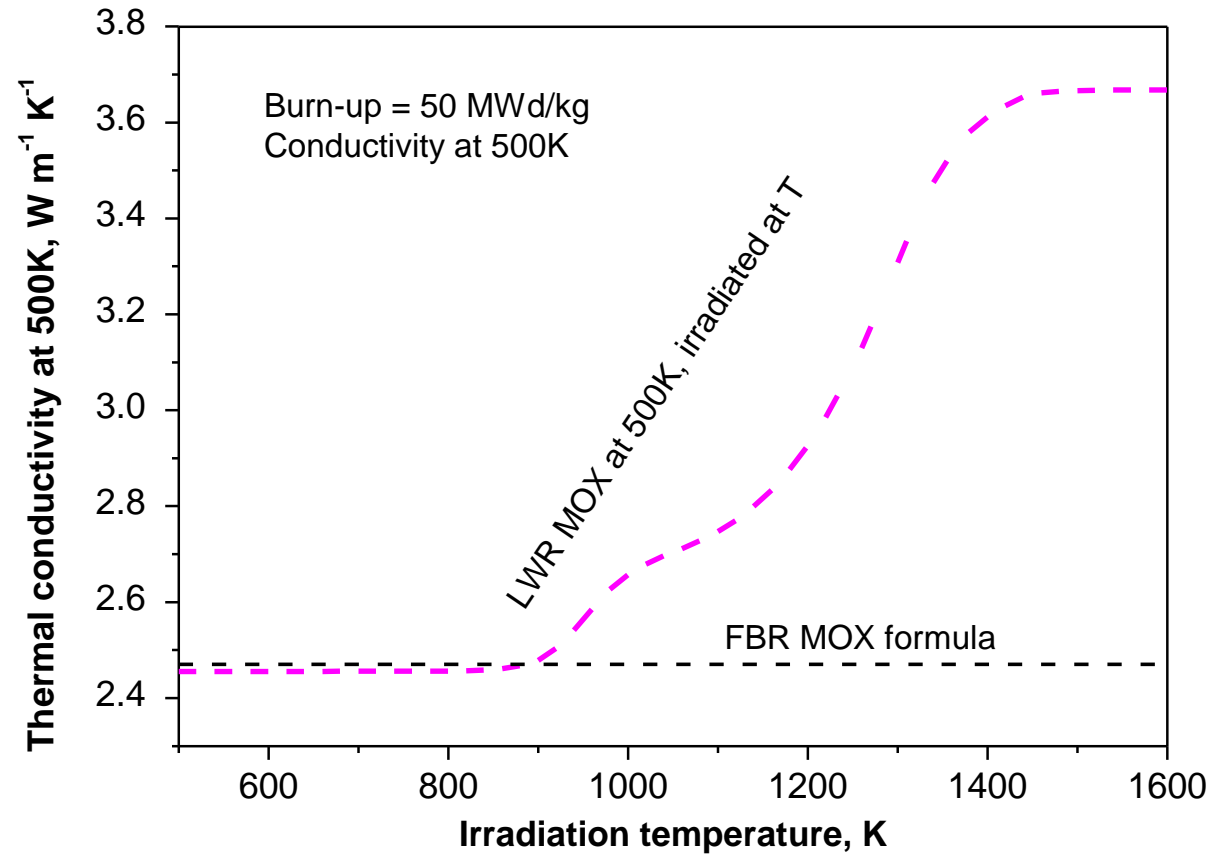
**FBR MOX
T range**

?

▨ λ at EOL; LOSSES DUE TO: ■ Rad. Damage ■ Fiss. Gas ■ Pores ■ Fiss. Products



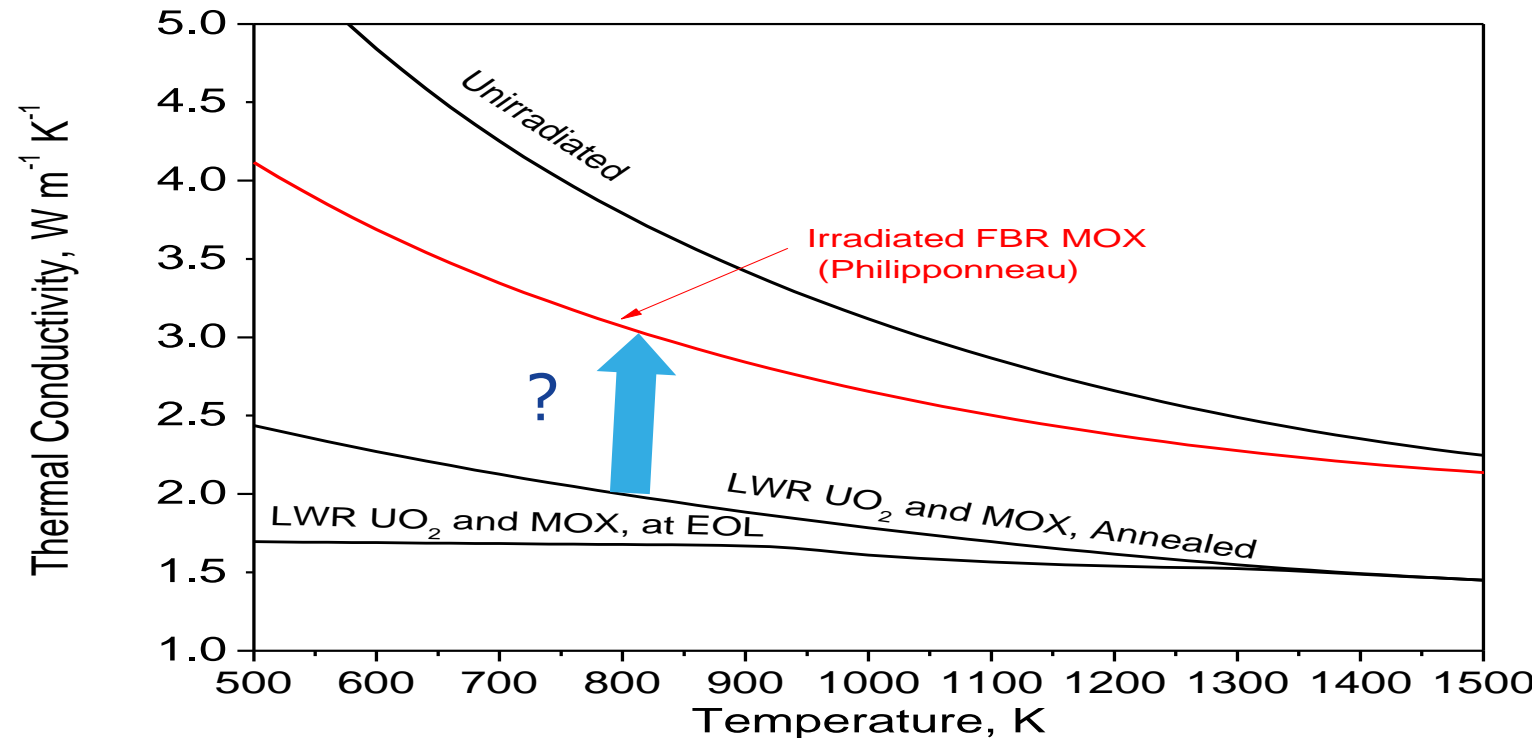
Stoichiometric irradiated LWR and FBR MOX fuels: annealing effects are known in LWR
MOX: conductivity at 500K is much higher if the fuel was irradiated at higher T





Degradation of the thermal conductivity during irradiation

- Measured high thermal conductivity values can not be explained by LWR fuel formulas by suppressing the contribution of radiation damage and fission gas.
- Agreement if FP effect reduced by 75%



- *The FP movement out of the fuel pellet and the presence of the JOG are proposed as main parameters*



- Oxide fuel shows extensive restructuring due to the high operating temperatures and the steep temperature gradient
- FR oxide fuel has a high fission gas release as a result of which the radiation induced swelling is limited
- Radial and axial redistribution of volatile fission products takes place
- A broad knowledge base for the properties of $(\text{U,Pu})\text{O}_2$ is available but still uncertainties exist, e.g. melting temperature and thermal conductivity

Thank you!

