

SOURCE TERMS

Sodium Fires & Aerosol Behavior

- I. Aerosol Generation (Pool Fires)***
- II. Current Code Predictability***

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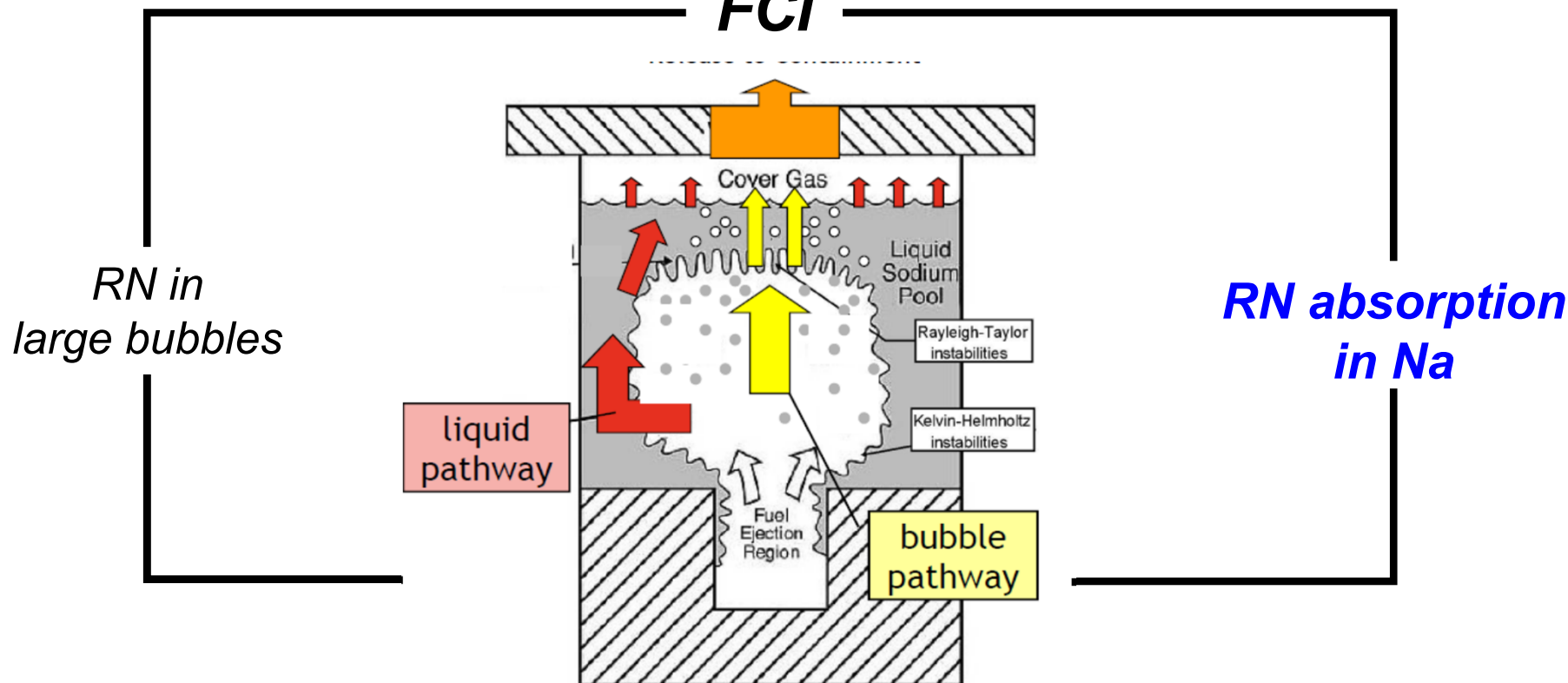
Background

BDBA Scenario

$$\uparrow T_{fuel}, \uparrow P_{rod}$$

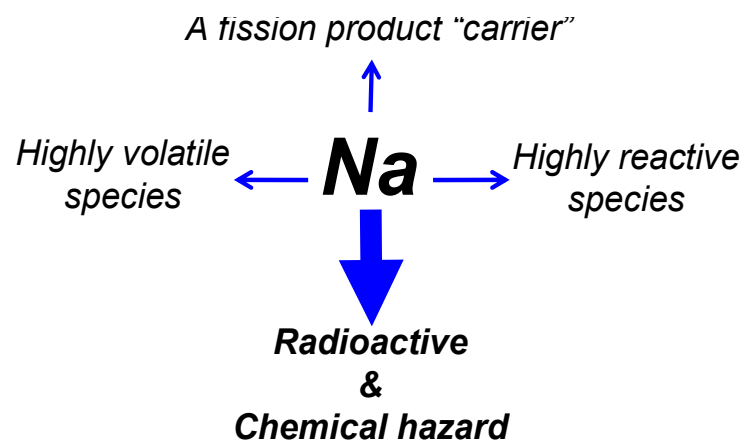
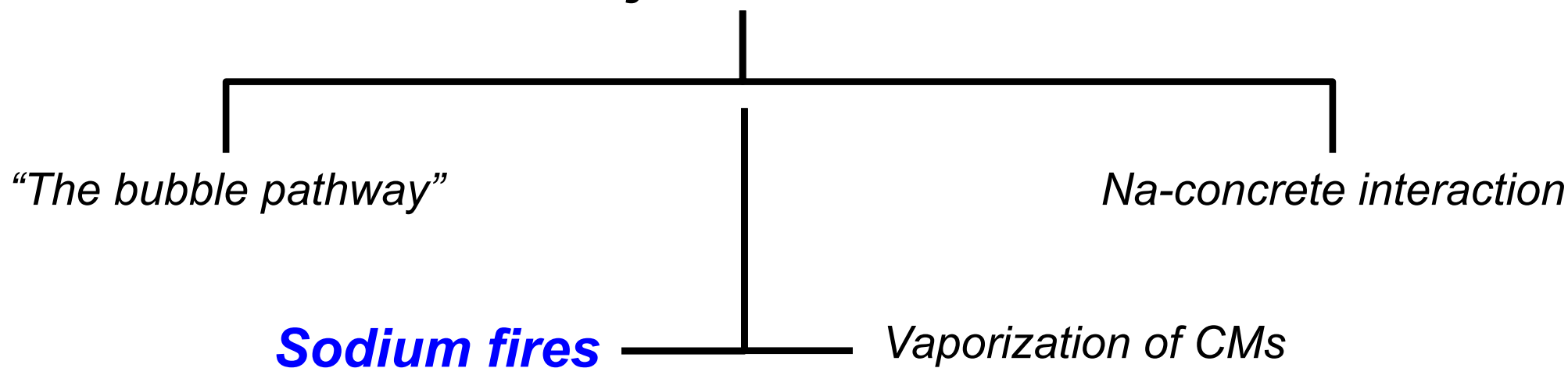
Core disruption

FCI



Background

Major Sources



Aerosol Generation (Pool Fires)

- ***Na Fires: Generic Analysis.***
- ***Aerosol Release & Transport.***



Na-Fires: Generic Analysis

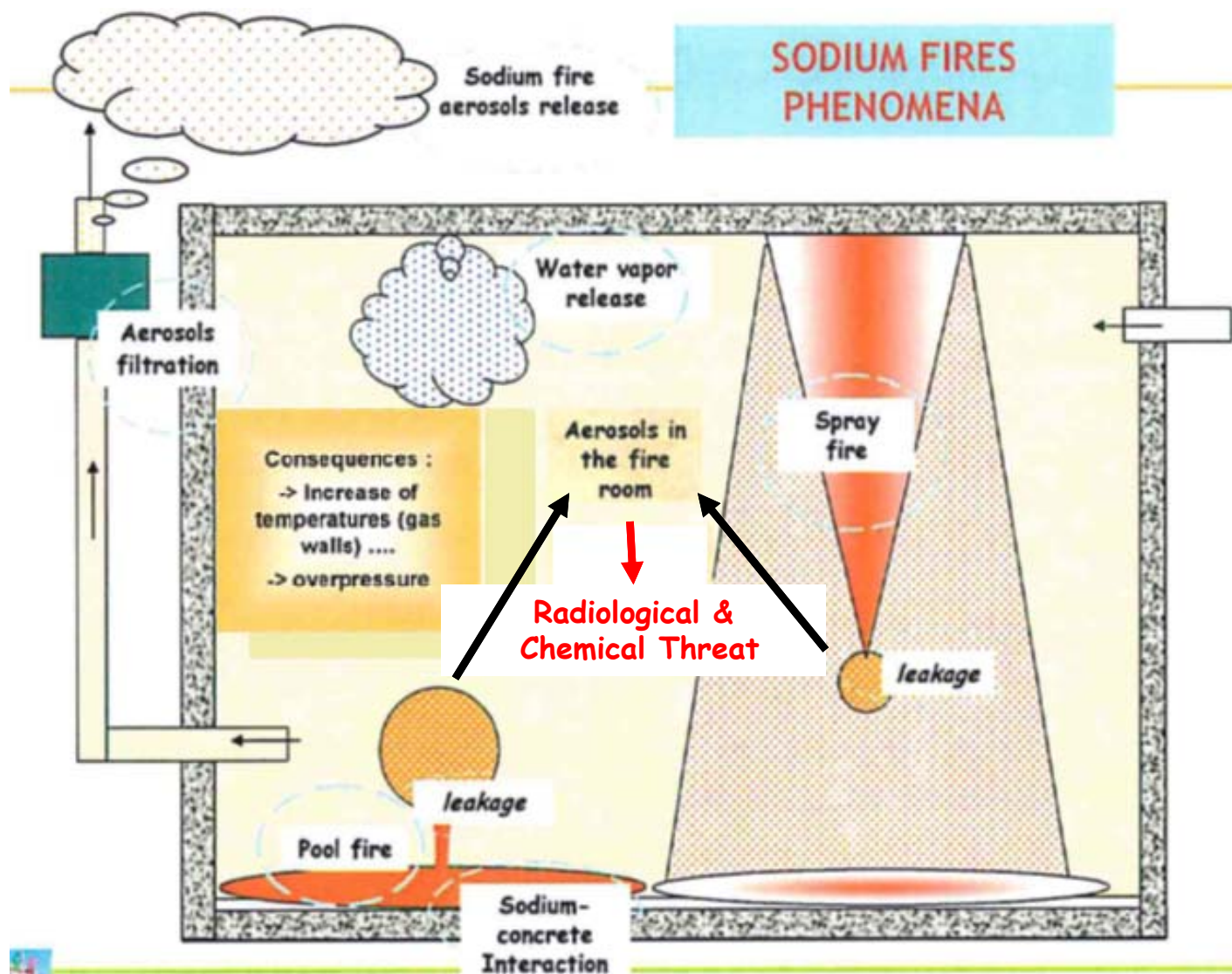


The Safety Issue

- **Sodium spills & fires pose a threat to plant safe operation**
 - **Thermal loads (P & T)** – sensible heat + combustion thermal energy.
 - **Na_xO_y – based particles** – radiological and chemical threat.
 - **RN partitioning & transport** – radiological threat.
- **Na-fire studies:**
 - Mangold & Tidball (1952); Charak & Smith (1965).
 - Atomics Intl. (1971); Hilliard et al. (1979).
 - Cherdron & Jordan (1980); Cherdron et al. (1985).
 - Lhiaubet et al. (1990); Malet et al. (1990); Souto et al. (1994).
 - Subramanian & Baskaran (2007); Subramanian et al. (2009).
 - ...
- **Na-fire codes:**
 - SOFIRE (Beiriger et al., 1973); CONTAIN-LMR (Murata, 1993).
 - SPM (Miyake, 1993); SOPA (Lee & Choi, 1997).
 - SPHINCS (Yamaguchi & Tajima, 2003).



Na-related Phenomena

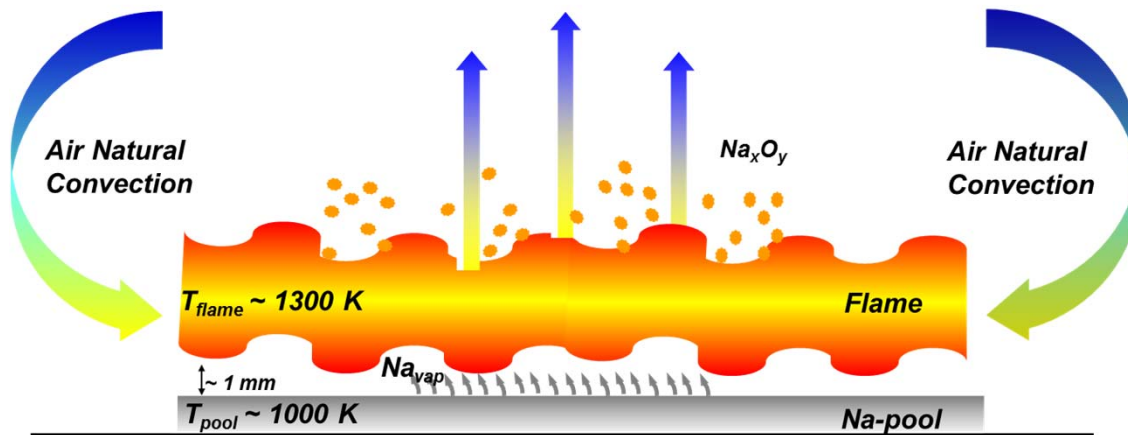


Casselmann, 2009

Configurations

Pool Fires

(Large breaks; $\sim 10^2$ kg/s)
(Low P spill)

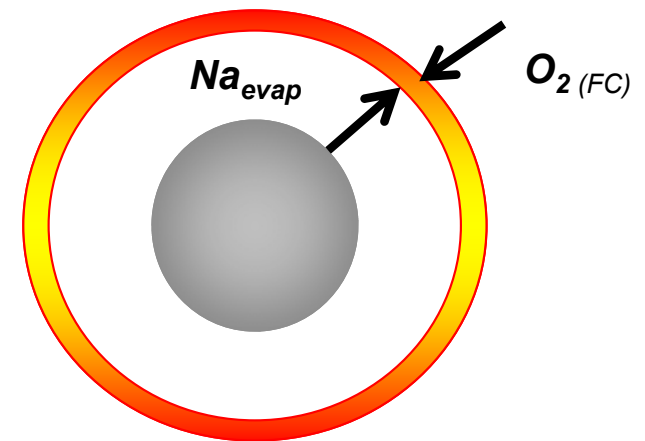


Surface reaction vs. **Gas-phase reaction**
(623 – 723 K)

Newman, 1983

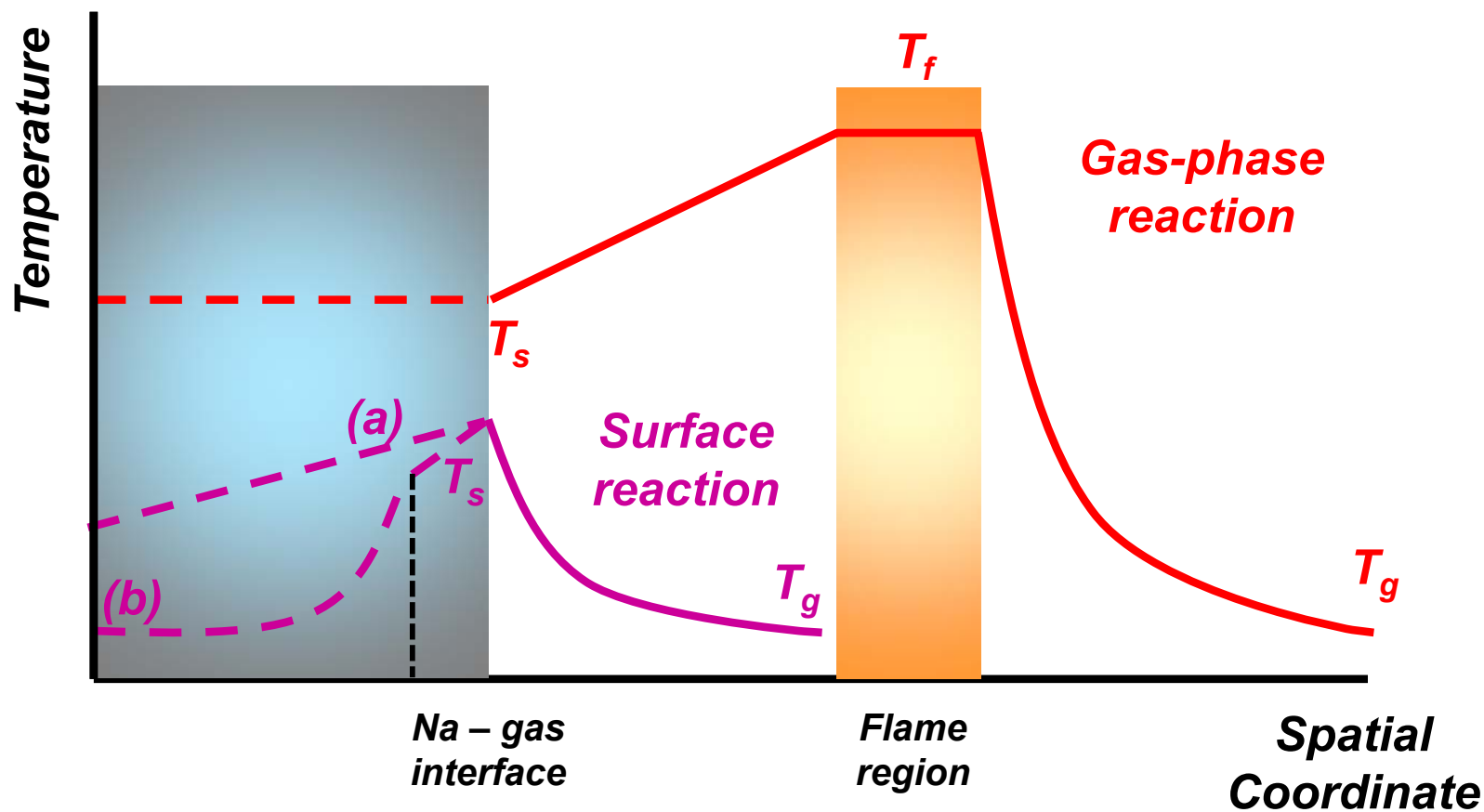
Spray Fires

(Smaller breaks; $\sim 10^0$ kg/s)



Jet hydrodynamics!
(jet fragmentation)

The Thermal Profile

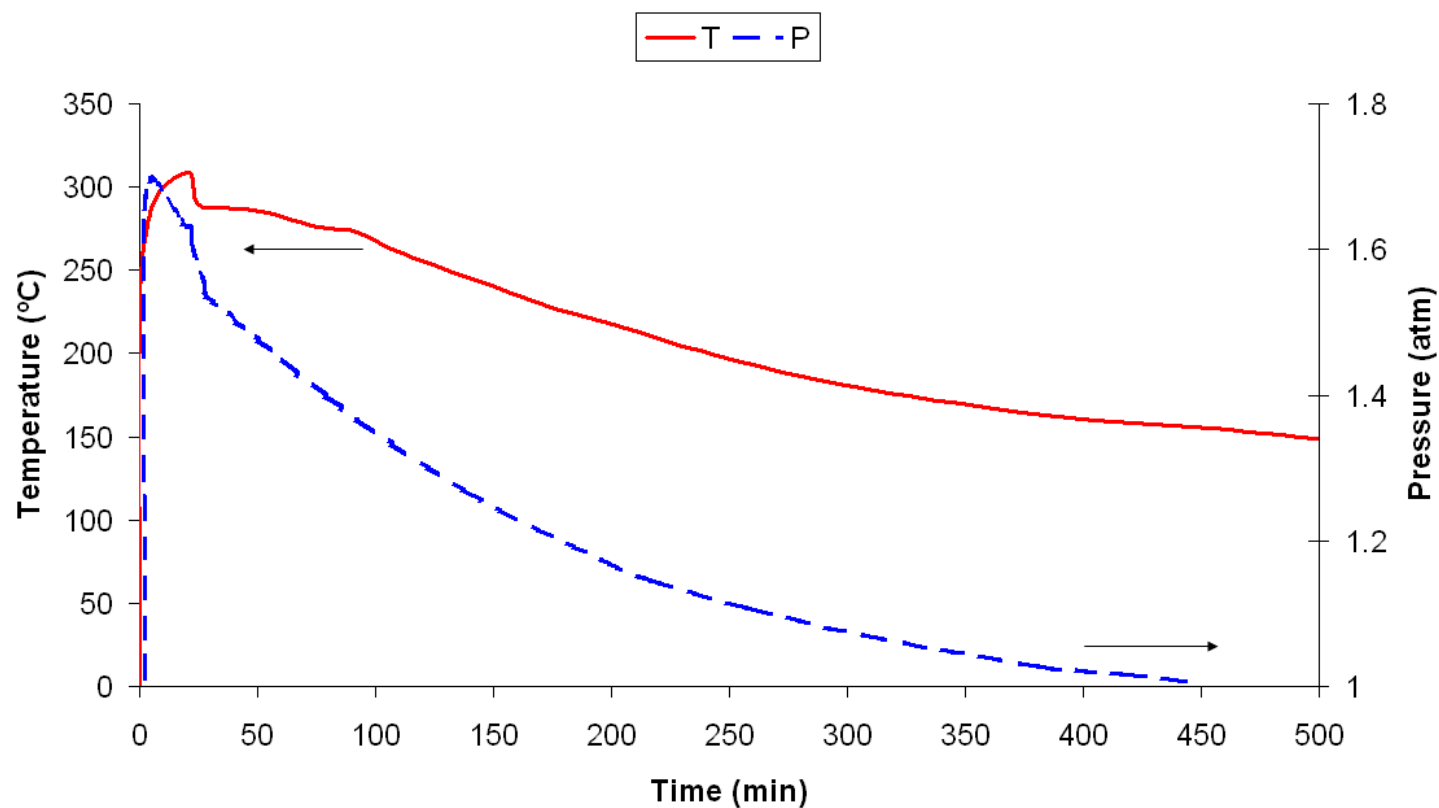


Reactions & Products

- $2 \cdot \text{Na} + 1/2 \cdot \text{O}_2 \rightarrow \text{Na}_2\text{O}$
 $\Delta h \sim 9.0 \text{ MJ/kg}$
 $T_m = 1132 \text{ }^\circ\text{C}$
 $T_b = 1950 \text{ }^\circ\text{C}$
- $2 \cdot \text{Na} + \text{O}_2 \rightarrow \text{Na}_2\text{O}_2$
 $\Delta h \sim 11.0 \text{ MJ/kg}$
 $T_m = 460 \text{ }^\circ\text{C}$
 $T_b = 657 \text{ }^\circ\text{C}$
- $\text{Na} + \text{H}_2\text{O}_v \rightarrow \text{NaOH} + 1/2 \cdot \text{H}_2$
 $\Delta h \sim 4.1 \text{ MJ/kg}$
- $\text{Na}_2\text{O} + \text{H}_2\text{O}_v \rightarrow 2 \cdot \text{NaOH}$
 $\Delta h \sim 4.2 \text{ MJ/kg}$
- $\text{Na}_2\text{O}_2 + \text{H}_2\text{O}_v \rightarrow 2 \cdot \text{NaOH} + 1/2 \cdot \text{O}_2$
 $\Delta h \sim 11.3 \text{ MJ/kg}$
- $2 \cdot \text{NaOH} + \text{CO}_2 \rightarrow \text{Na}_2\text{CO}_3 + \text{H}_2\text{O}$
 $\Delta h \sim 3.6 \text{ MJ/kg}$



Pool Fire

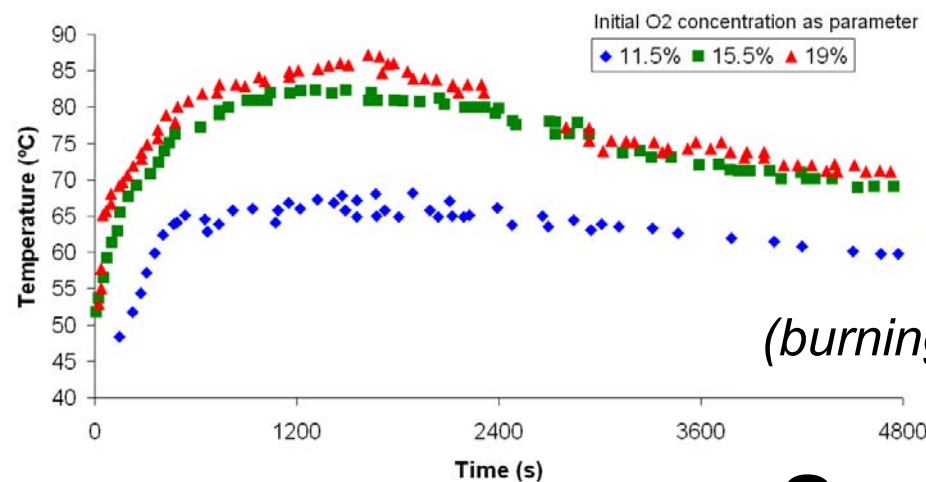


**Chiao, 1994
(CONTAIN-LMR)**

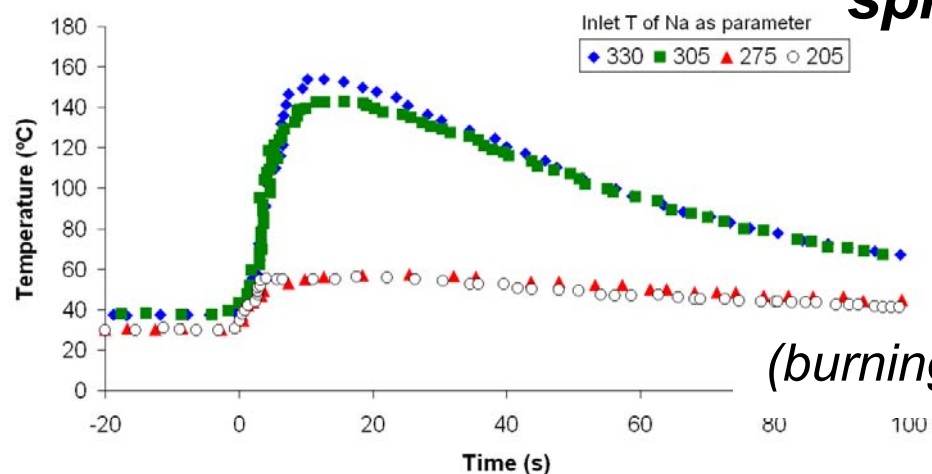
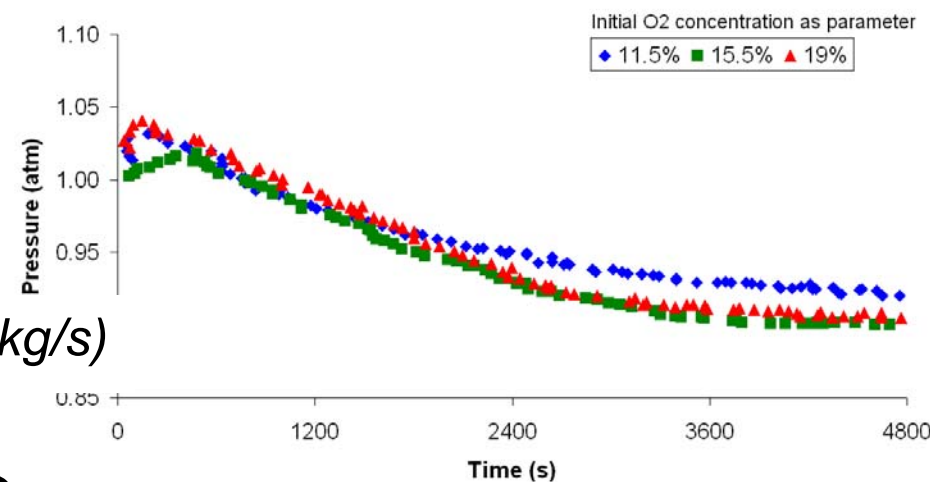
Natural circulation → Quasi-homogeneous atmosphere



Pool Fires vs. Spray Fires

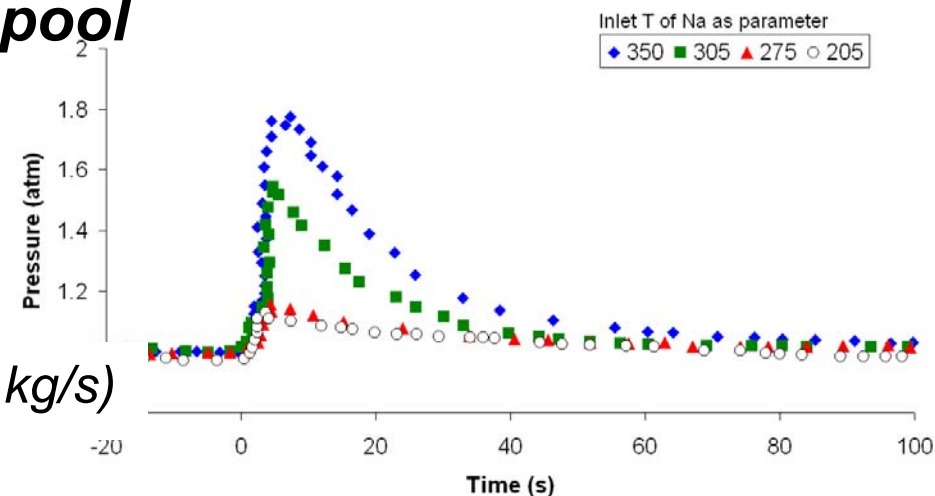


Pool
(burning rate ~ 0.1 kg/s)

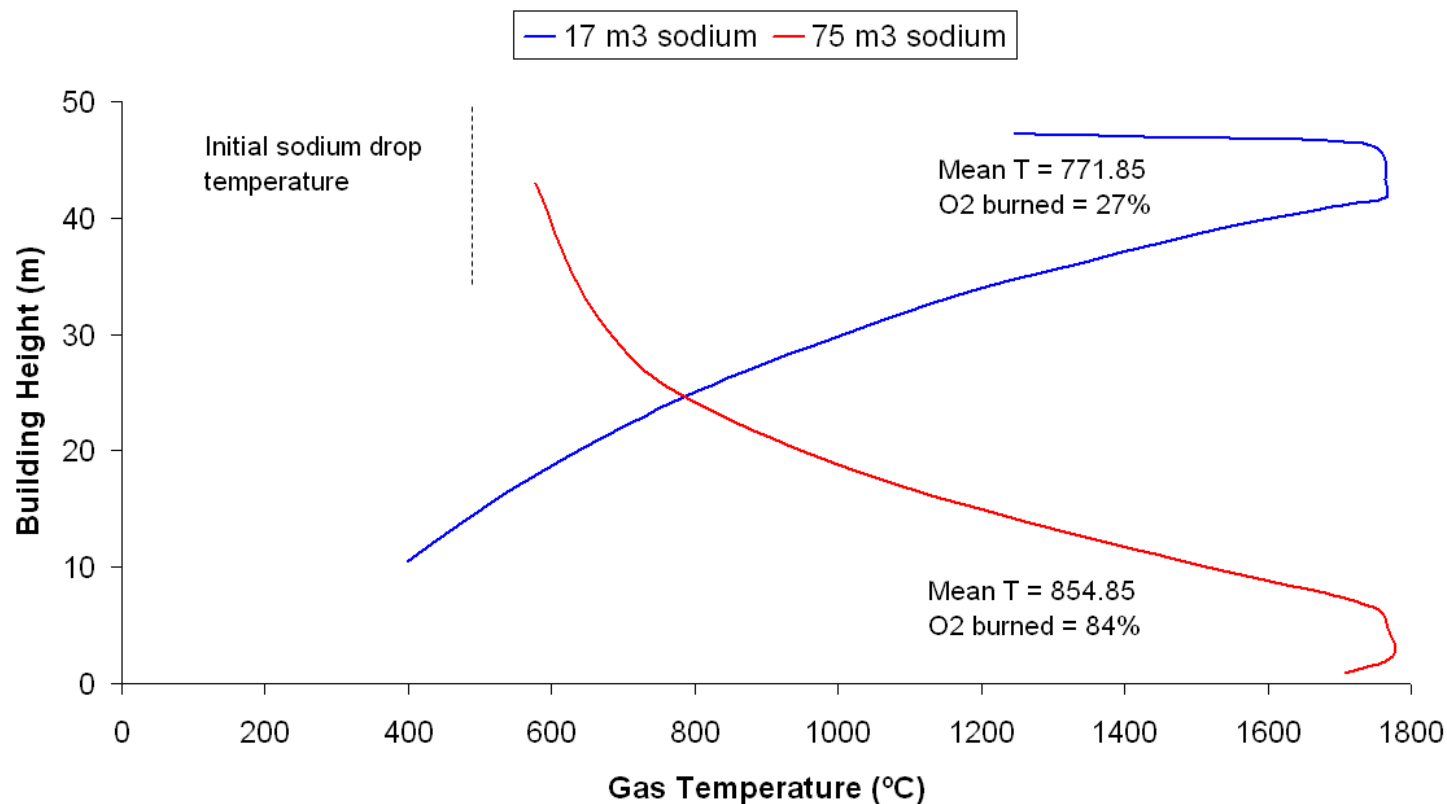


$S_{\text{spray}} \gg S_{\text{pool}}$

Spray
(burning rate $\sim n \cdot 10$ kg/s)



Spray Fires



**Heisler, 1979
(SOMIX)**

Highly non-uniform atmosphere → Large thermal gradients



Take Aways

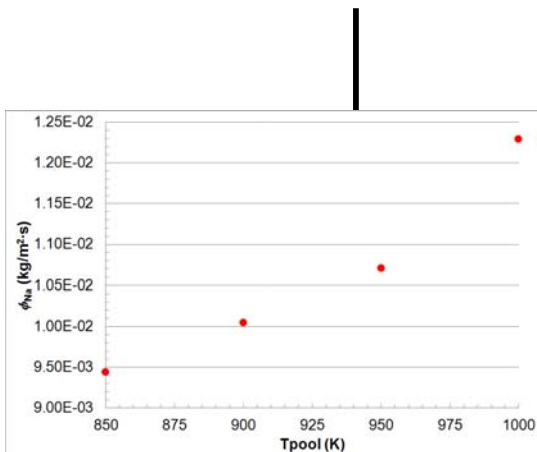
- ***Therm. & mech. loads of pool/spray fires are largely different.***
- ***Spray therm. & mech. loads are notably higher and faster.***
- ***Even in the case of sprays, $P_{max} < P_{limit}$***
- ***Sprays involve large thermal gradients.***
- ***$t(P_{max}) \neq t(T_{max})$ in pools (burning rate vs. heat removal rate).***

Aerosol Release & Transport

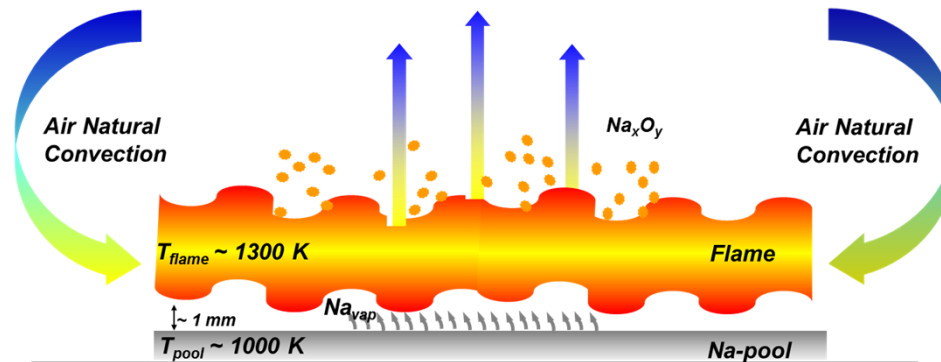
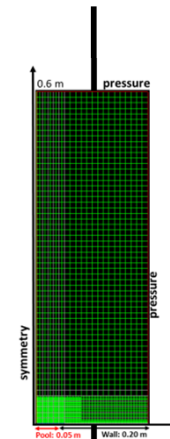


Particle Generation: Phenomena

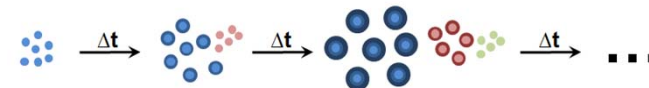
Na Supply
(Evaporation Model)



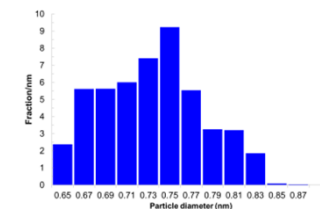
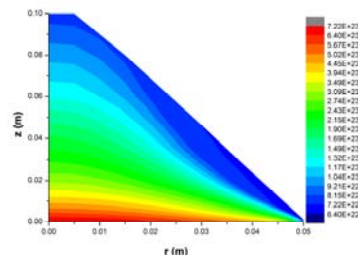
O₂ Supply
(3D Convective Modeling)



Formation of Na_xO_y Vapors
(Na – O₂ chemical reactions)



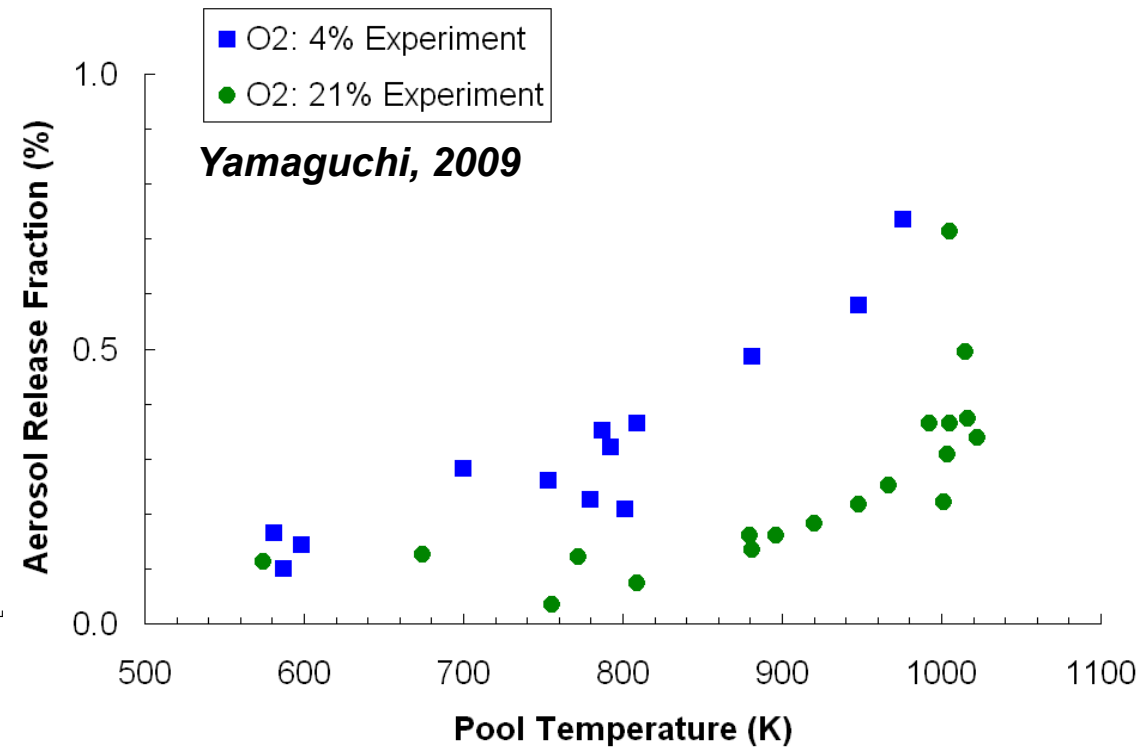
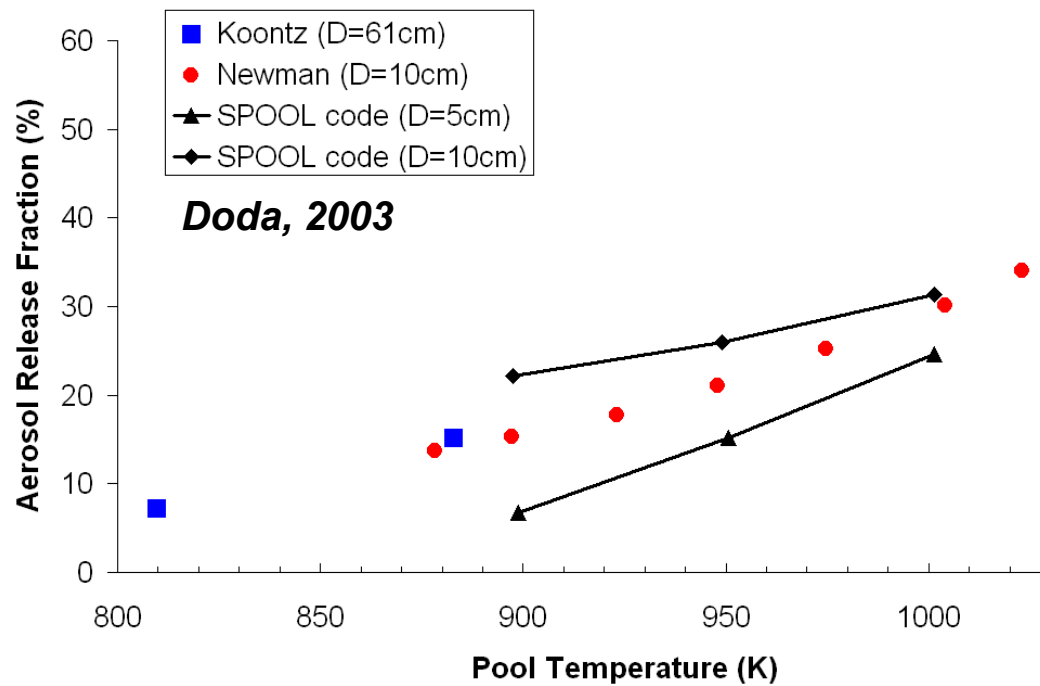
Generation of Primary Particles
(Nucleation & Growth models)



García, 2016



Aerosol Release



$$N = c_1 \cdot \dot{m}_{vap} \cdot d_{pool}^{c2} \cdot X_{O_2}^{c3}$$



Aerosol Size

NEA, 1979

Reference	Material	Primary particle diameter, μm
Allent & Briant	Mixed UO_2 , PuO_2	Log-normal, bimodal, ($\sigma_g=1.35$) 0.003-.01
Chatfield	Pu , Na	0.02 maximum
Castleman	Mixed UO_2 , PuO_2	Log-normal, 0.004-.004, $\sigma_g=2.0$
	PuO_2	0.1, ($\sigma_g=1.9$)
	UO_2 , Na	0.2-0.6
Morrison et al.	Clad & bare UO_2	0.002-0.1
Kelly et al.	UO_2	<0.005-0.02
Jordan et al.	UO_2	$d_g=0.073$ ($\sigma_g=1.85$)
Kres	UO_2 , U_3O_8	0.014-0.034
Kitani	U_3O_8	$d_g=0.037$ ($\sigma_g=1.6-2.2$)
	U_3O_8	$d_g=0.07$ ($\sigma_g=1.93$)
Schikarski	Clad mixed	<0.08
	Oxide fuel	
	Na_2O	0.1-0.4
Hilliard et al.	Na_2O_2 , NaOH	0.1-0.5
Parker et al.	UO_2 , U_3O_8	$d_g=0.034$

AMMD ~ 0.5 -1.0 μm (GSD ~ 2)

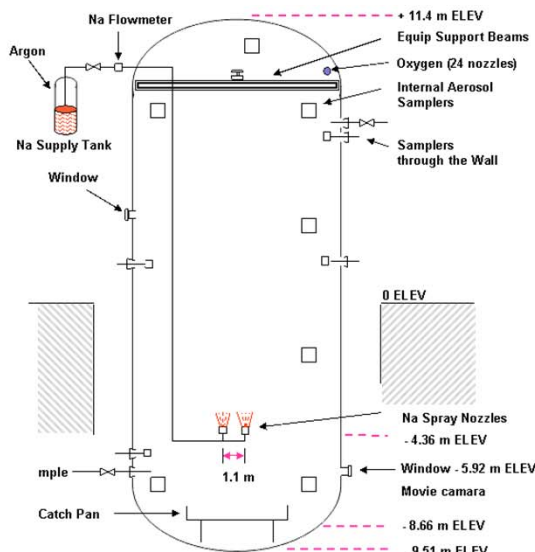
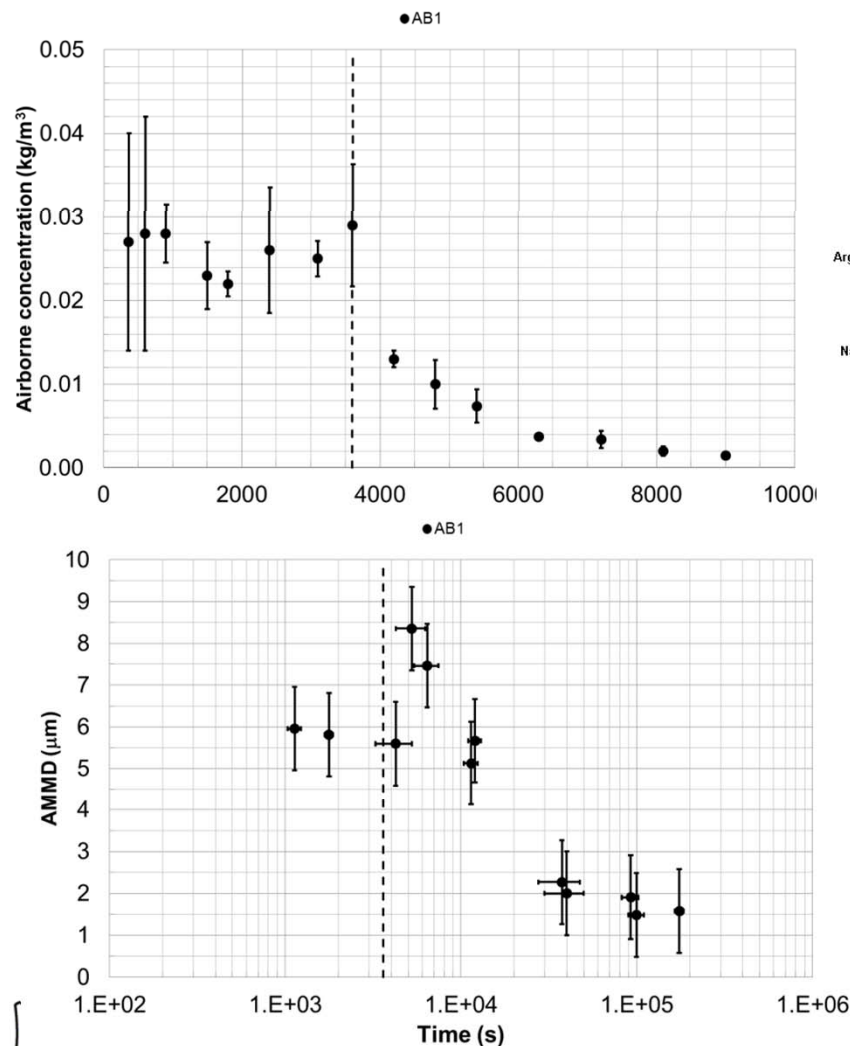
Cherdron, 1985

Jordan, 1988

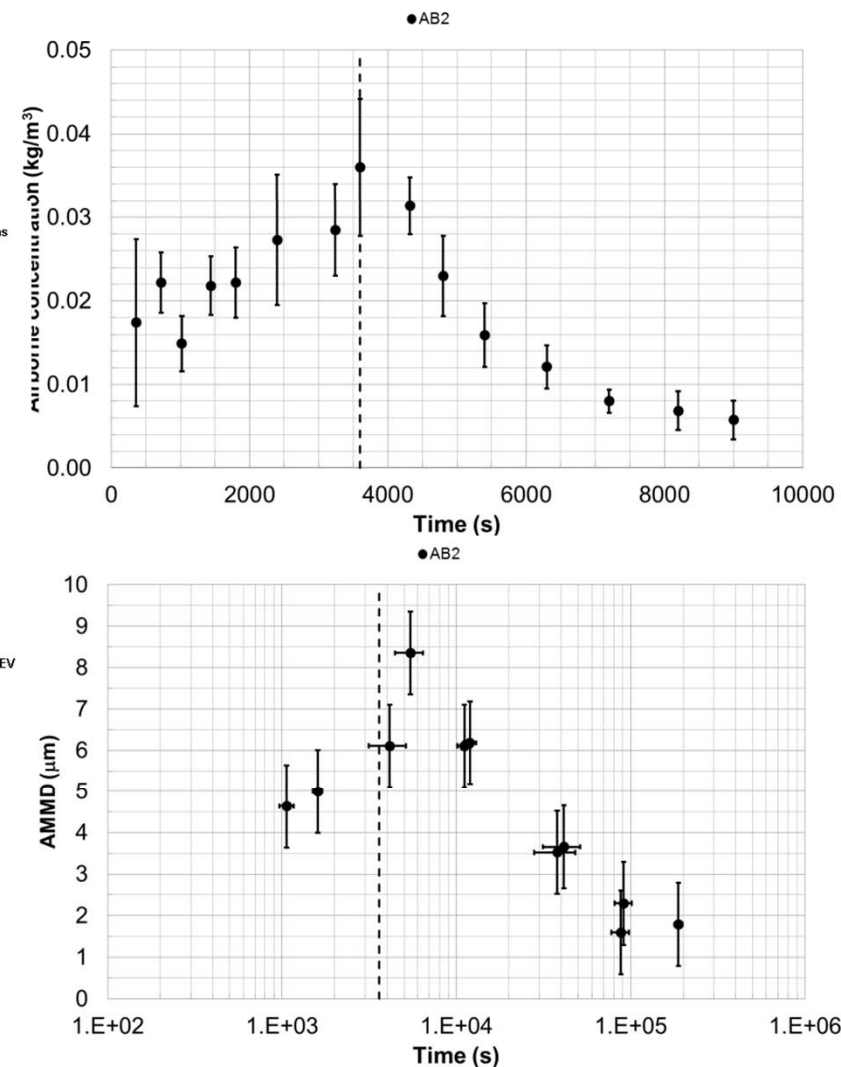
Subramanian, 2007

Online, March 30th 2021

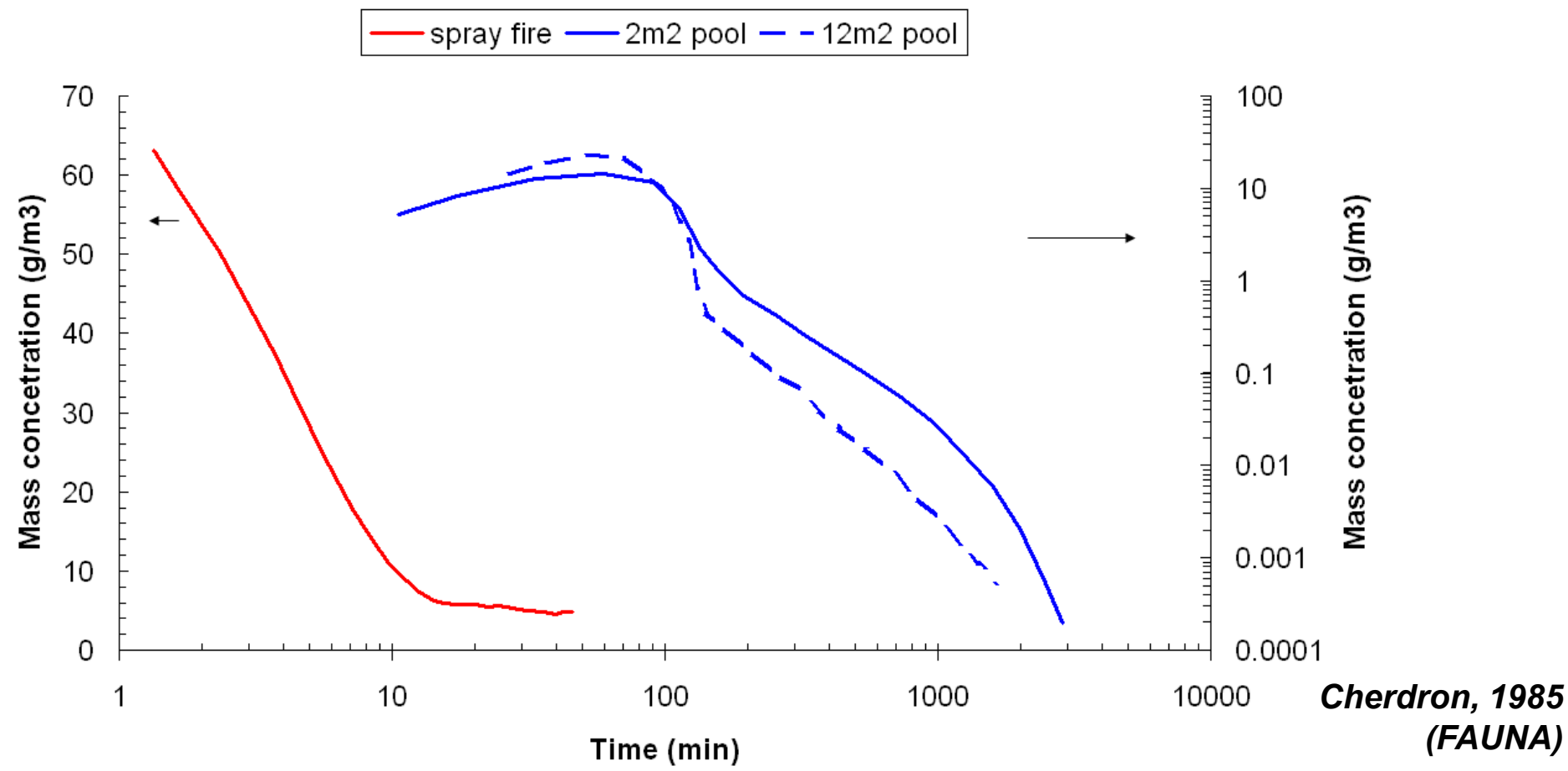
Aerosol Evolution (I)



Hilliard, 1977
McCormack, 1979



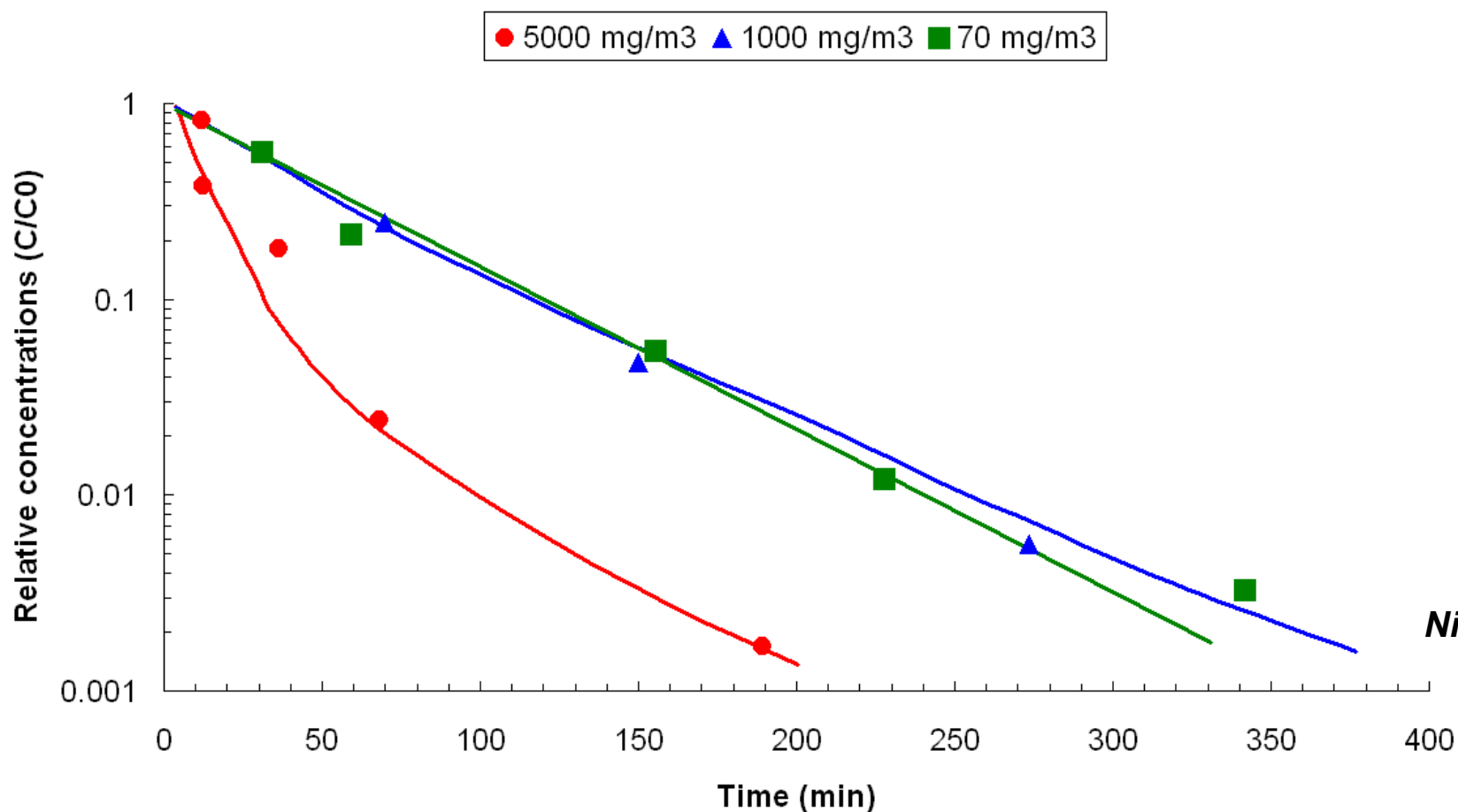
Pool vs. Sprays



- Much lower concentration!
- 100 times slower depletion!



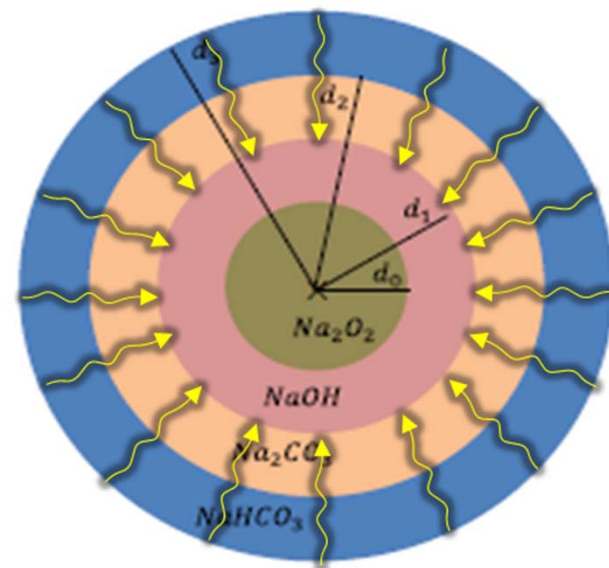
Interaction Processes



Nishio, 1977

Na_xO_y Particle Chemistry

- $Na_2O + H_2O_v \rightarrow 2 \cdot NaOH$ $\Delta h \sim 4.20 \text{ MJ/kg}$
- $Na_2O_2 + H_2O_v \rightarrow 2 \cdot NaOH + \frac{1}{2} \cdot O_2$ $\Delta h \sim 11.28 \text{ MJ/kg}$
- $2 \cdot NaOH + CO_2 \rightarrow Na_2CO_3 + H_2O$ $\Delta h \sim 3.6 \text{ MJ/kg}$
- $Na_2CO_3 + H_2O + CO_2 \rightarrow 2 \cdot NaHCO_3$ $\Delta h \sim 3.6 \text{ MJ/kg}$



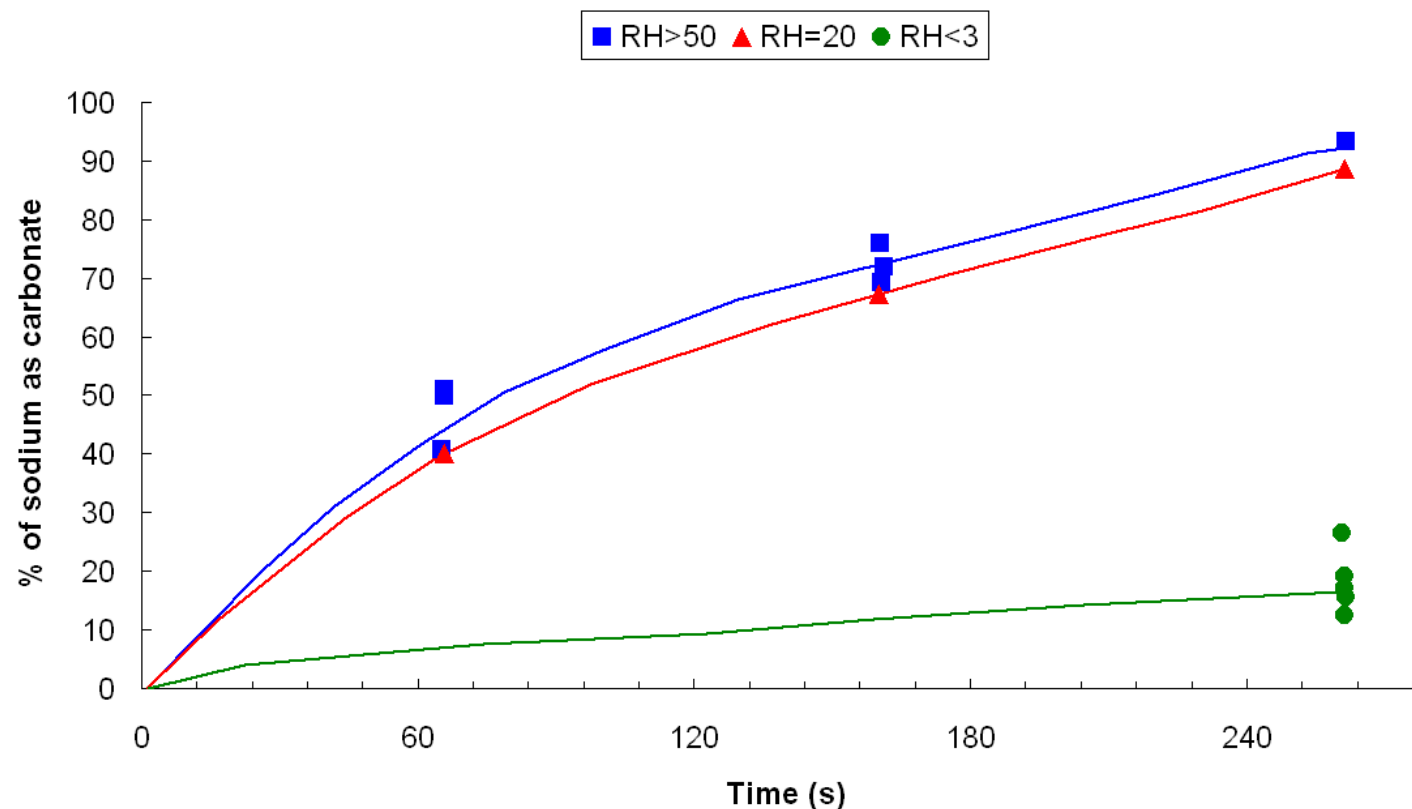
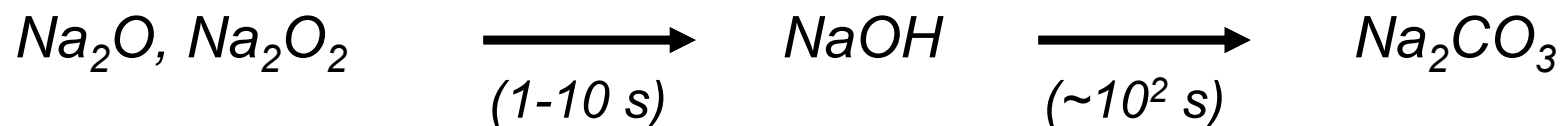
$$W_i = \frac{2\pi c_i D_i^* d_i d_p f}{d_p - d_i}$$

$$D_K^* = \frac{194 e^2 d'}{6 \tau (1 - e)} \sqrt{\frac{T}{M}}$$

Cooper, 1980

Mathé, 2016

Aerosol Chemical Speciation



Cherdron, 1985

Take Aways

- ***Large amounts of aerosols may be generated.***
- ***Sprays burning produces higher aerosol concentrations.***
- ***Airborne residence time depends on conditions ([particles]).***
- ***Aerosol aging is a key process (non-radiological effects).***
- ***Failure of components & plugging of filters.***



Current Code Predictability

- ***Na Containment Database.***
- ***Analytical Modeling.***
- ***Results and Discussion.***

Herranz et al. (2018), “Progress in modeling in-containment source term with ASTEC-Na”, ANUCENE 12, 84-93.

Herranz et al. (2017), “In-containment source term predictability of ASTEC-Na: Major insights from data-predictions benchmarking”, NED 320, 269-281

Herranz et al. (2013), “Benchmarking LWR codes capability to model radionuclide deposition within SFR containments: An analysis of the Na ABCOVE tests”, NED 265, 772-784.



Take Aways

- *Scarcity of available experimental data (fundamental & integral).*
- *Single node approximation good enough.*
- *Codes capture the trends, but through heavy parametrization!*
- *Data uncertainties hinder specific Na-models insights.*

Major Model Needs in Na Source Term Analysis

- ***Particle generation** from pool and **spray** fires.*
- ***RN partitioning** between gas and condensed phases.*
- ***Chemical reactivity** of RNs and Na compounds.*
- ***Validation** of any modeling through SETs and ITs.*

SUMMARY

- ***Na fires are a distinguishing feature of SFRs.***
- ***Na-fire aerosols dominate radiological and chemical threat.***
- ***Na-fires are major source of aerosol generation.***
- ***Na-based aerosol physics is similar to LWR aerosols***
- ***Particle chemistry is essential to estimate SFR risk.***
- ***Scarcity & uncertainties of experimental data!***
- ***“ST Codes” capture the trends through heavy parametrization!***
- ***FP radiological impact dominated by Cs.***

Thank you for your attention!
Any questions?

